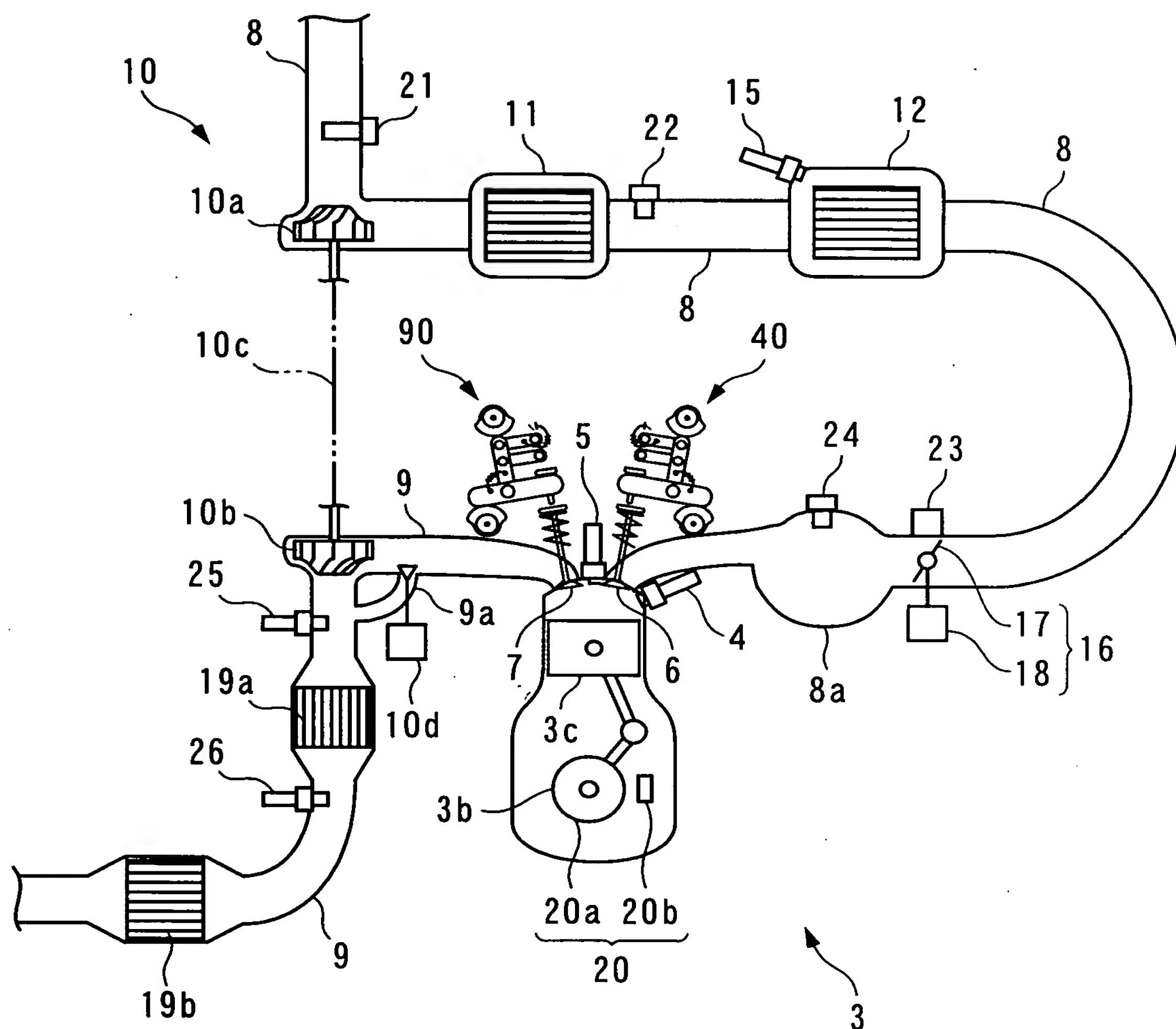
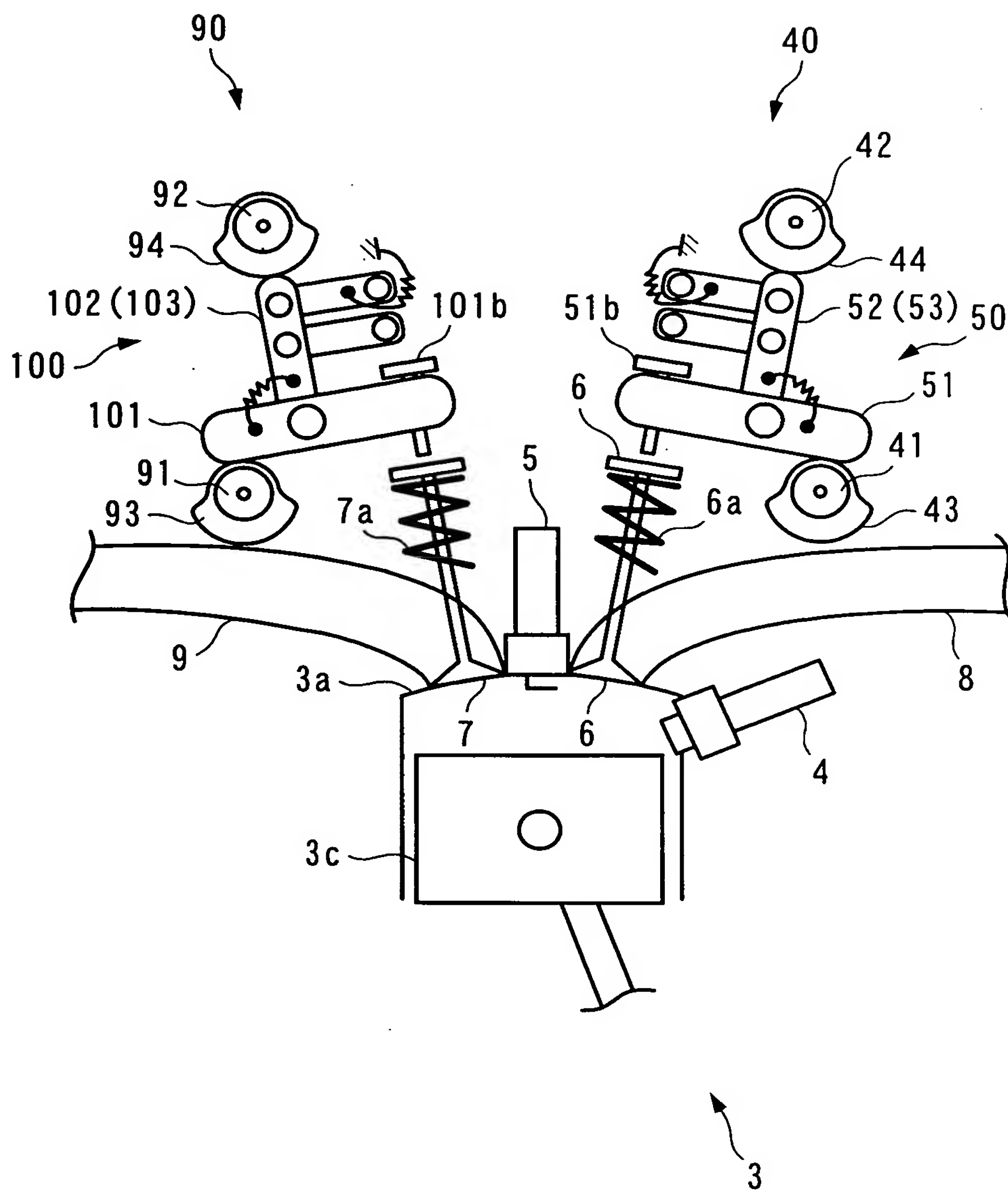


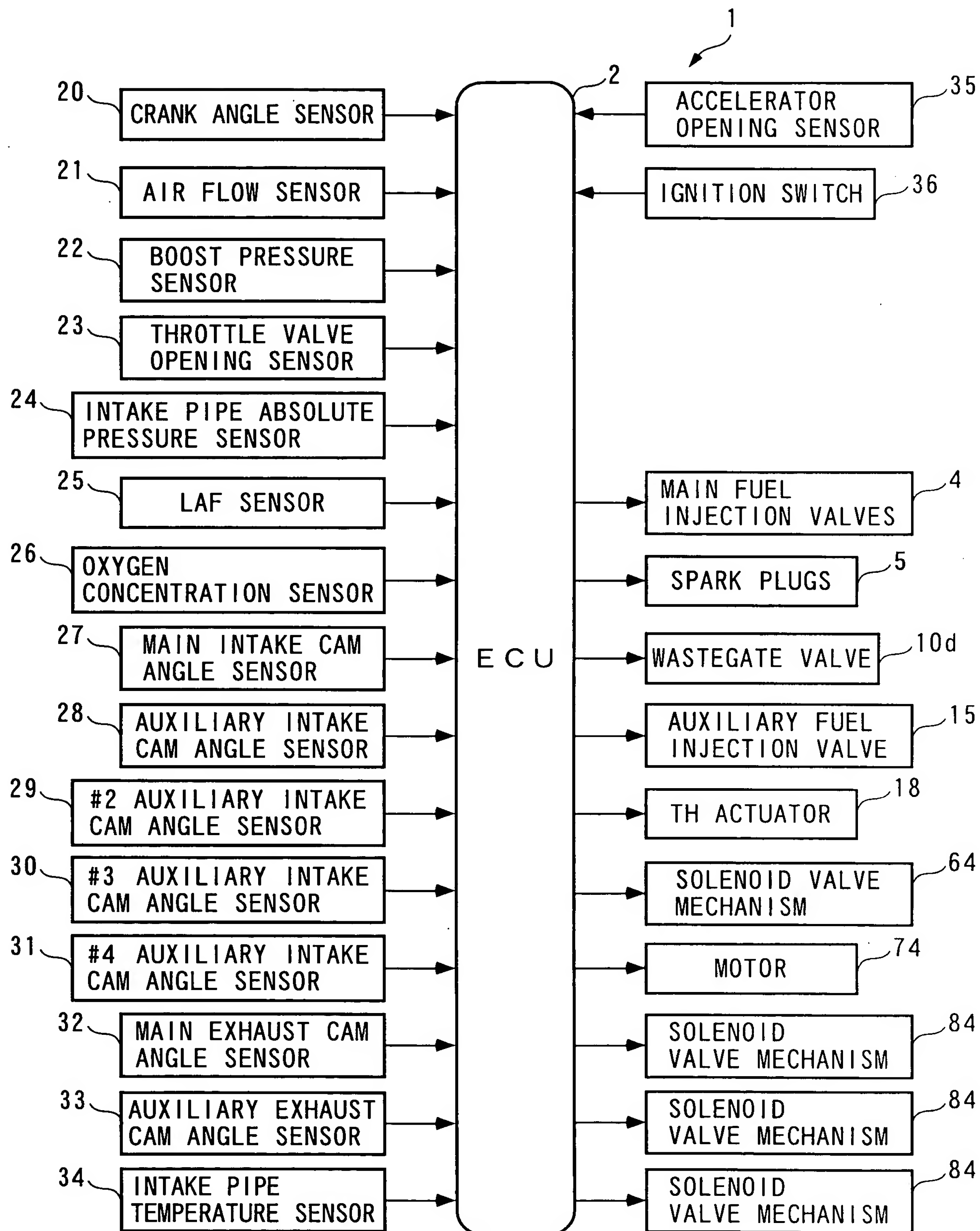
FIG. 1



F I G. 2



F I G . 3



F I G . 4

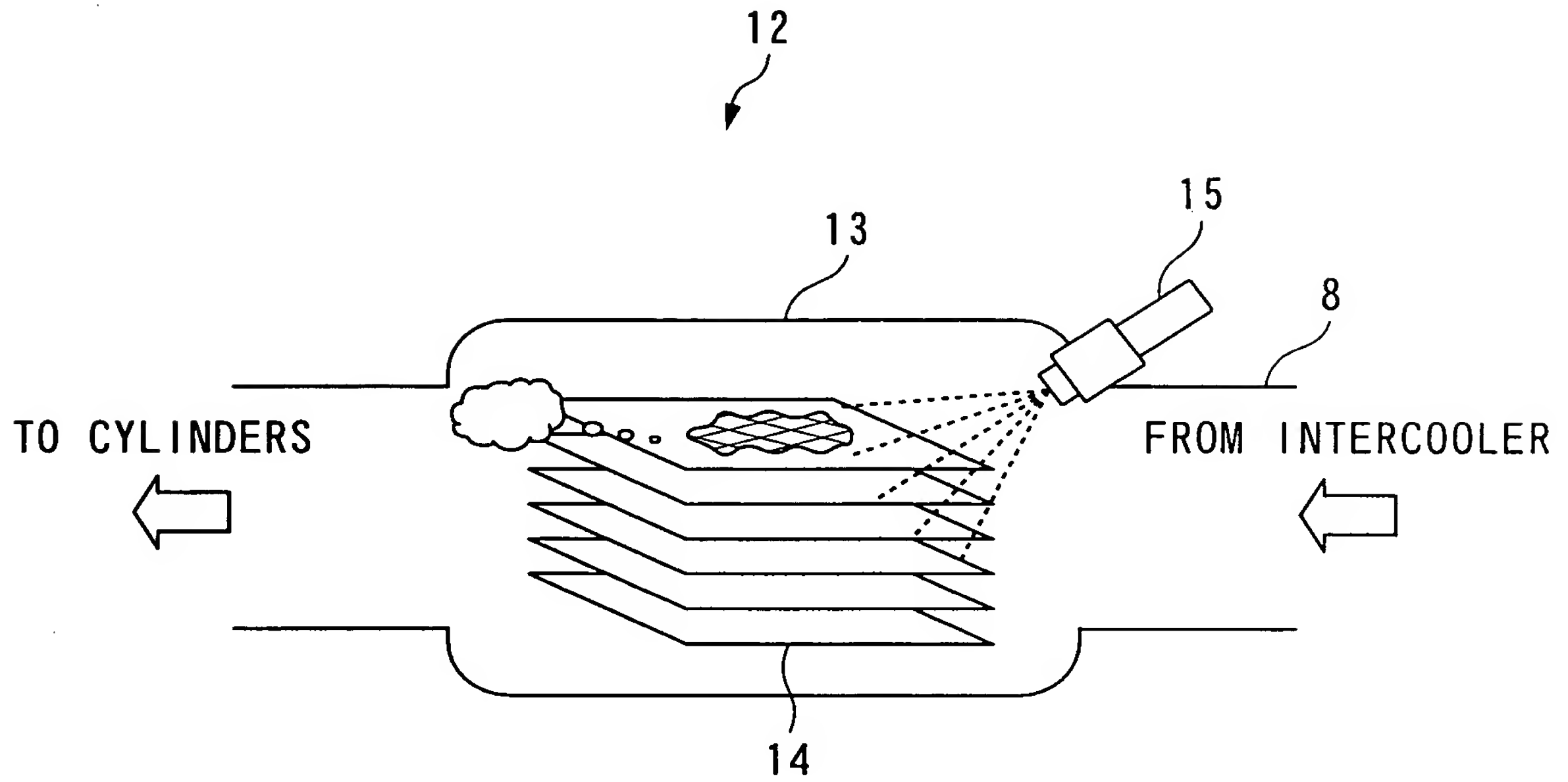
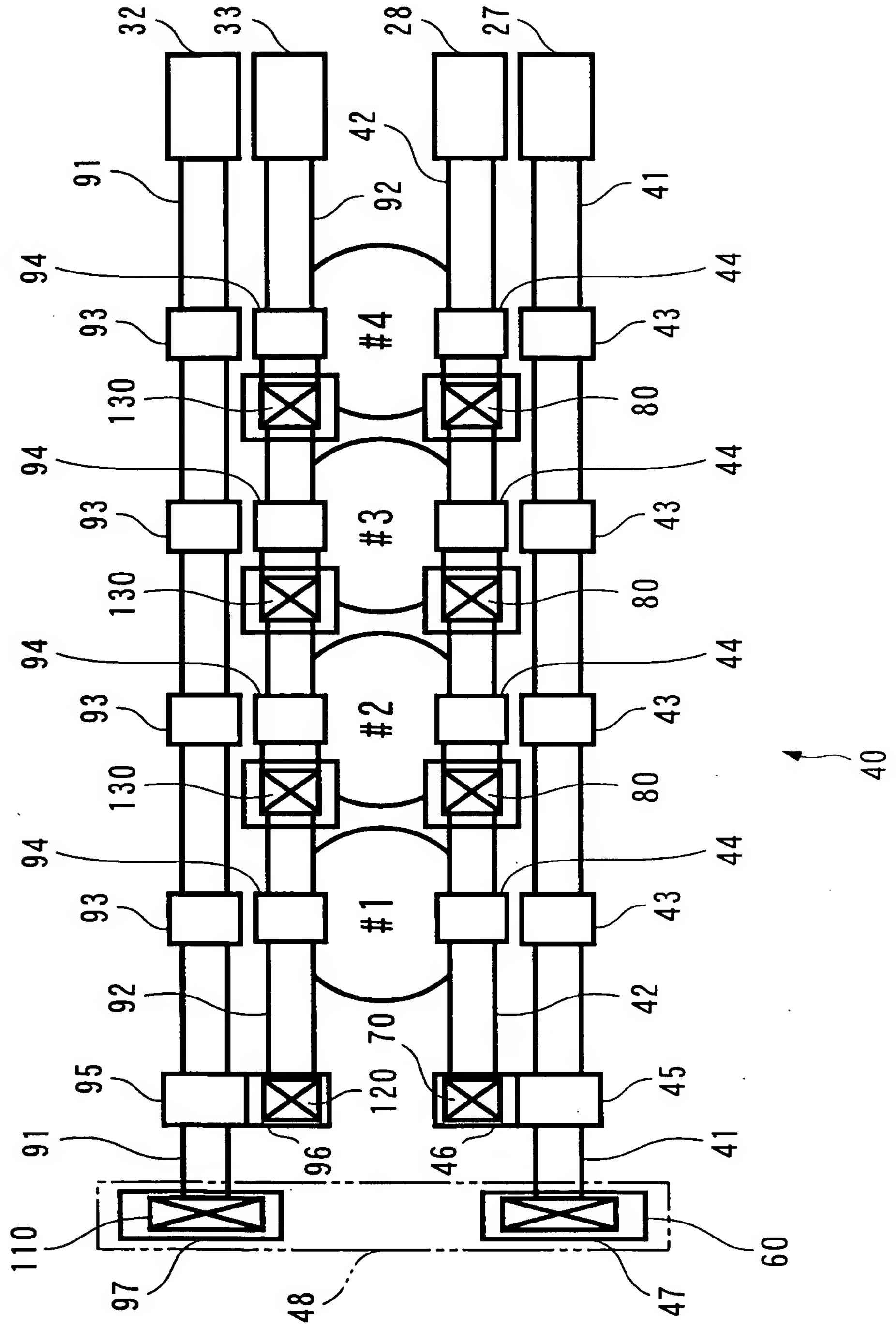
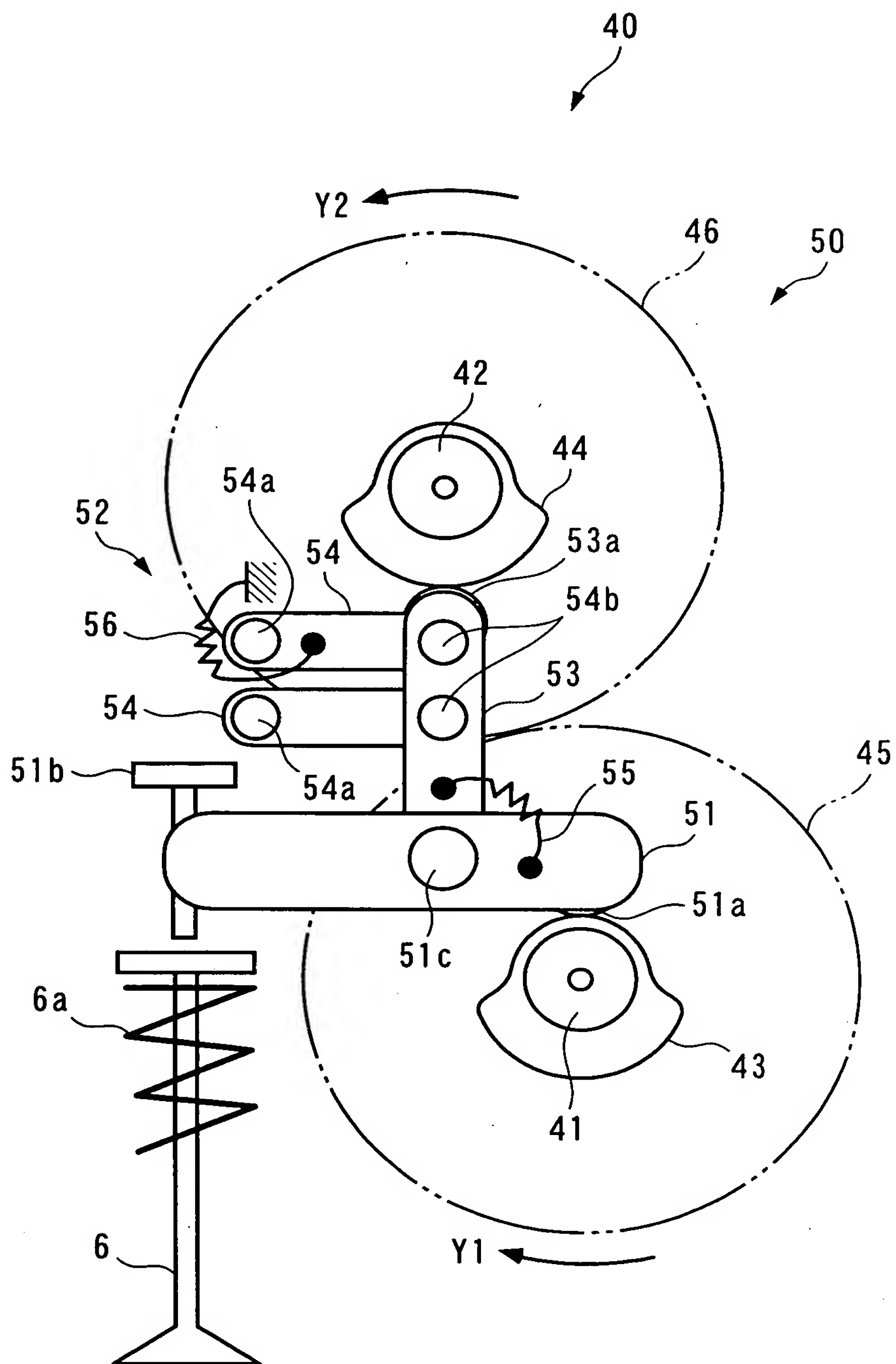


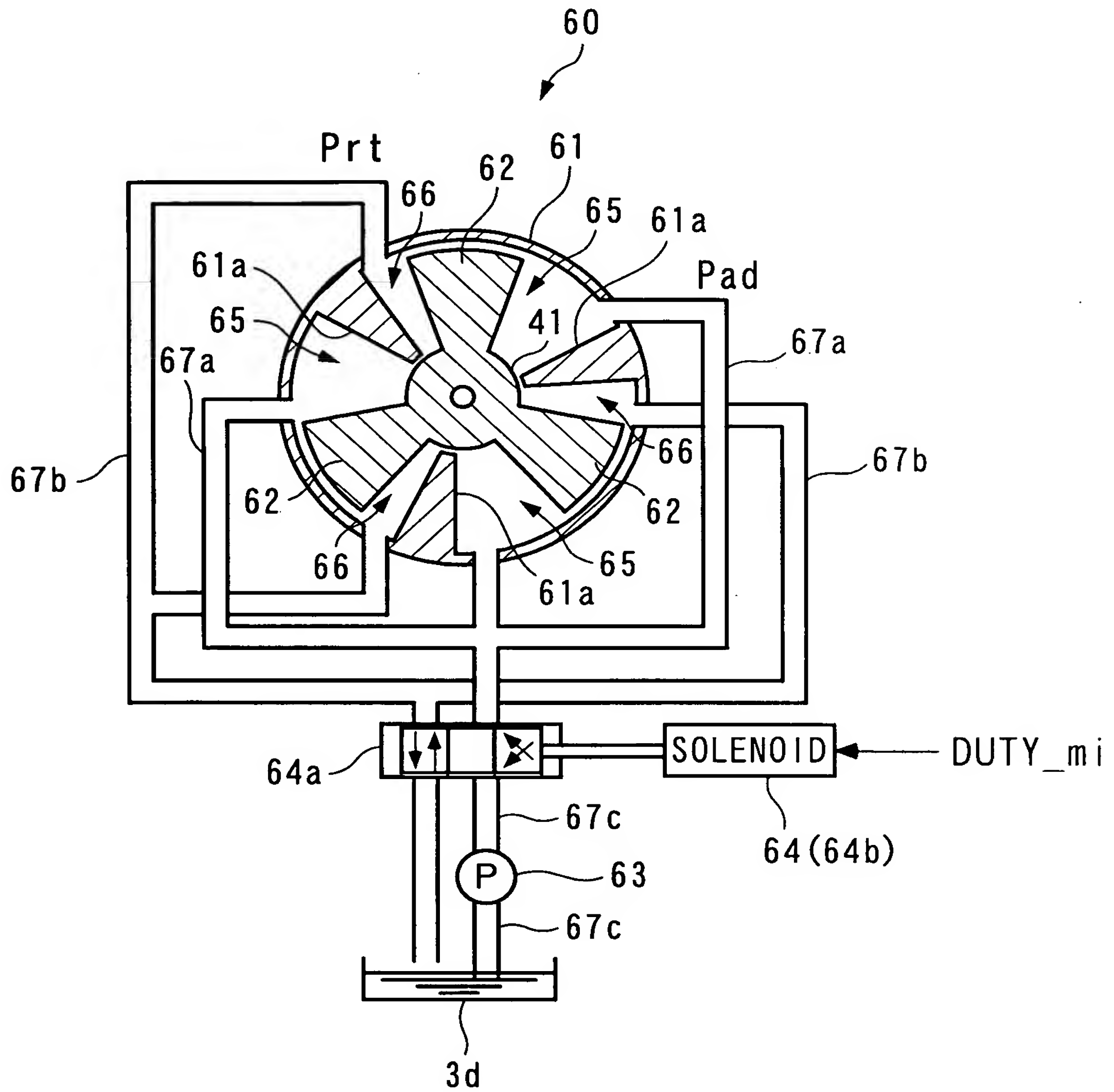
FIG. 5



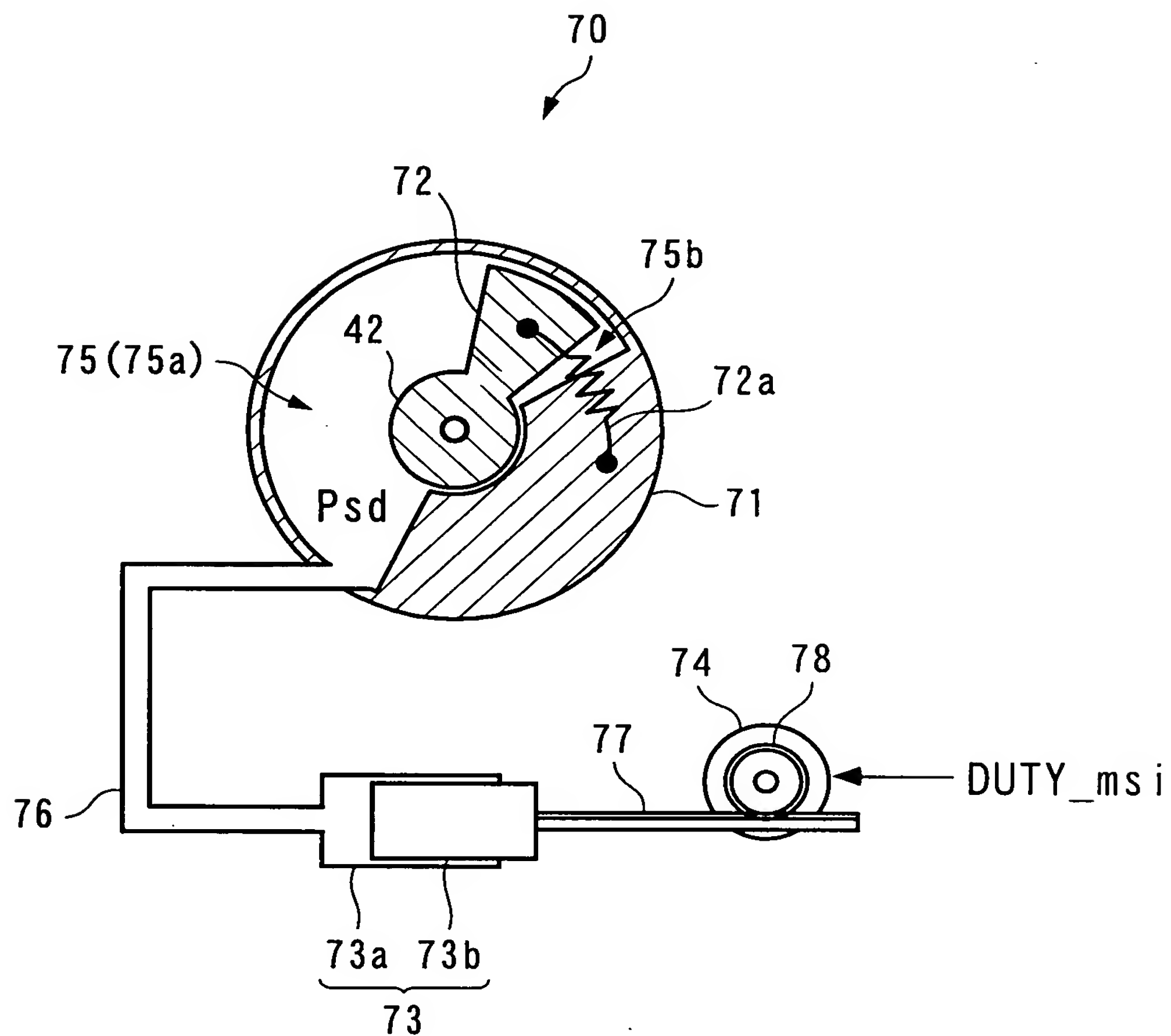
F I G . 6



F I G. 7

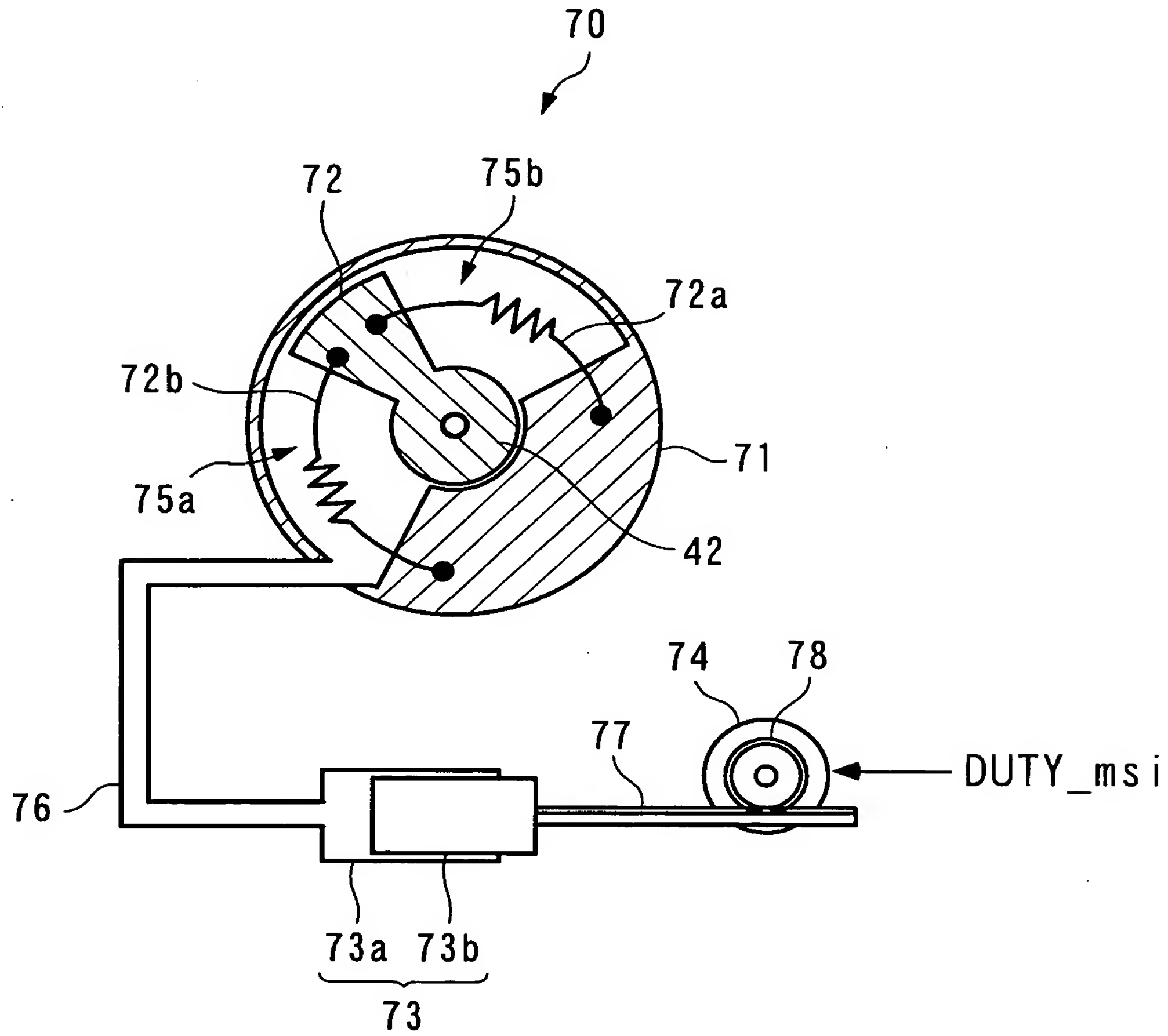


F I G . 8





F I G. 9



F I G. 1 0

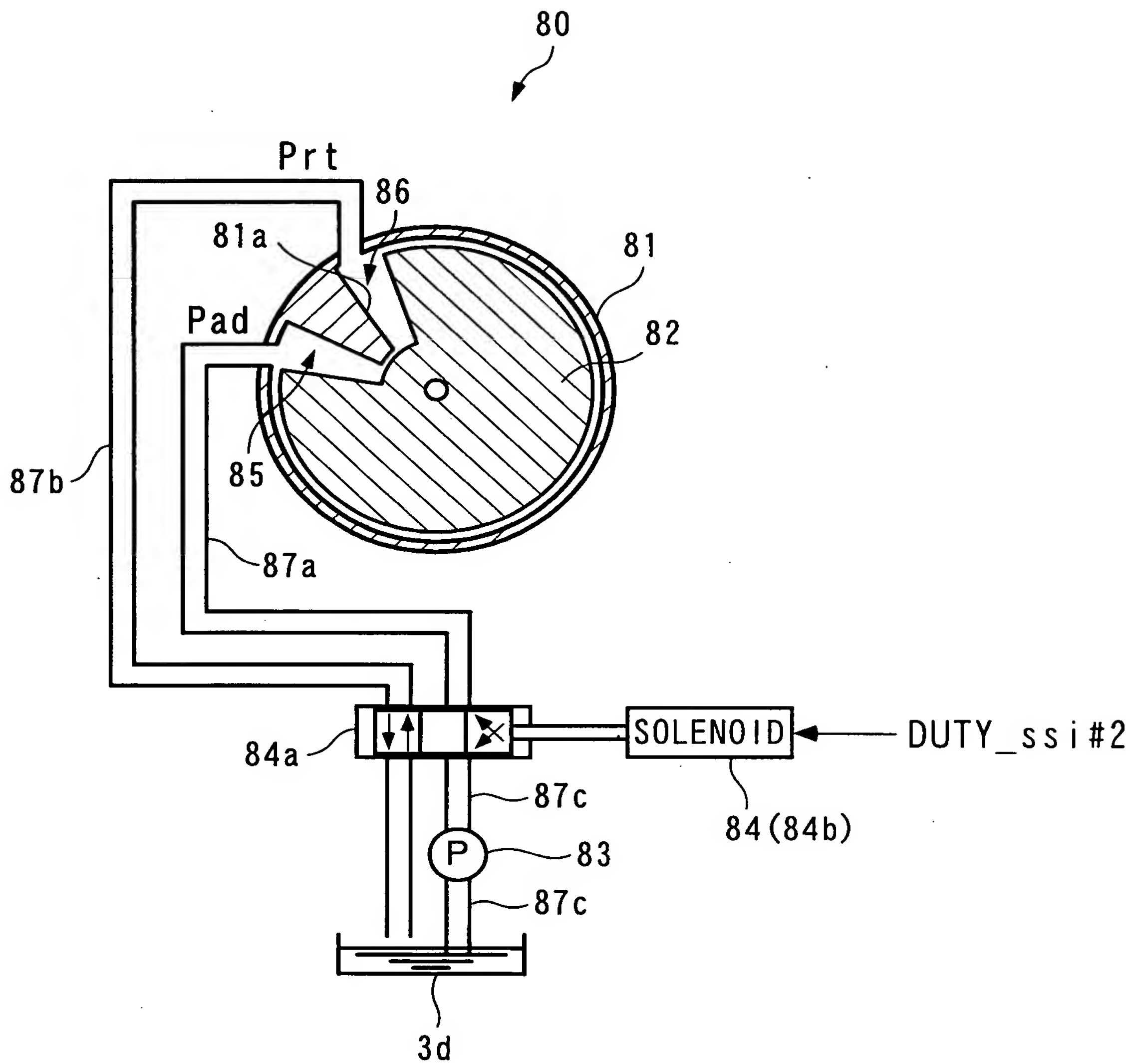
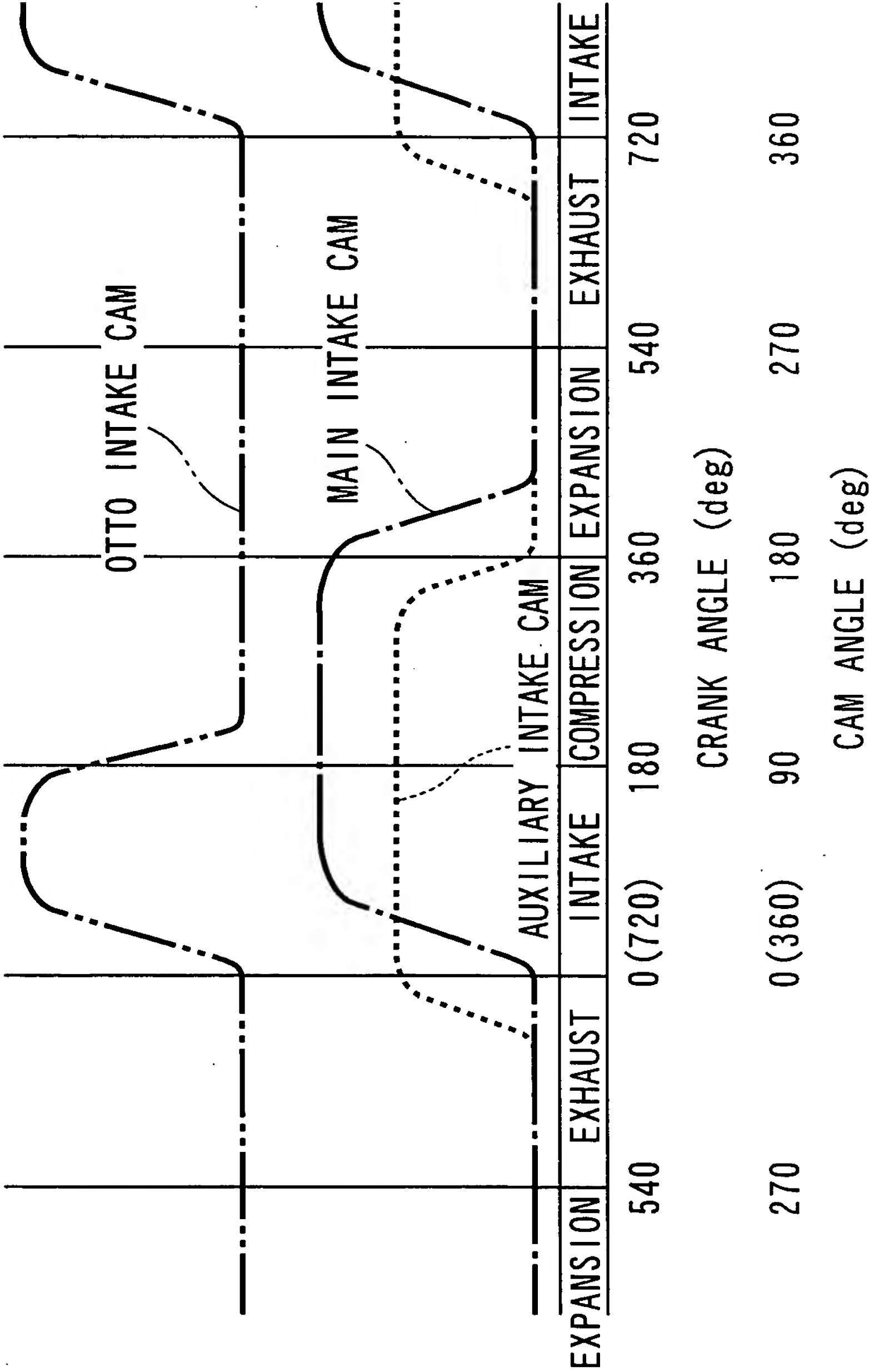
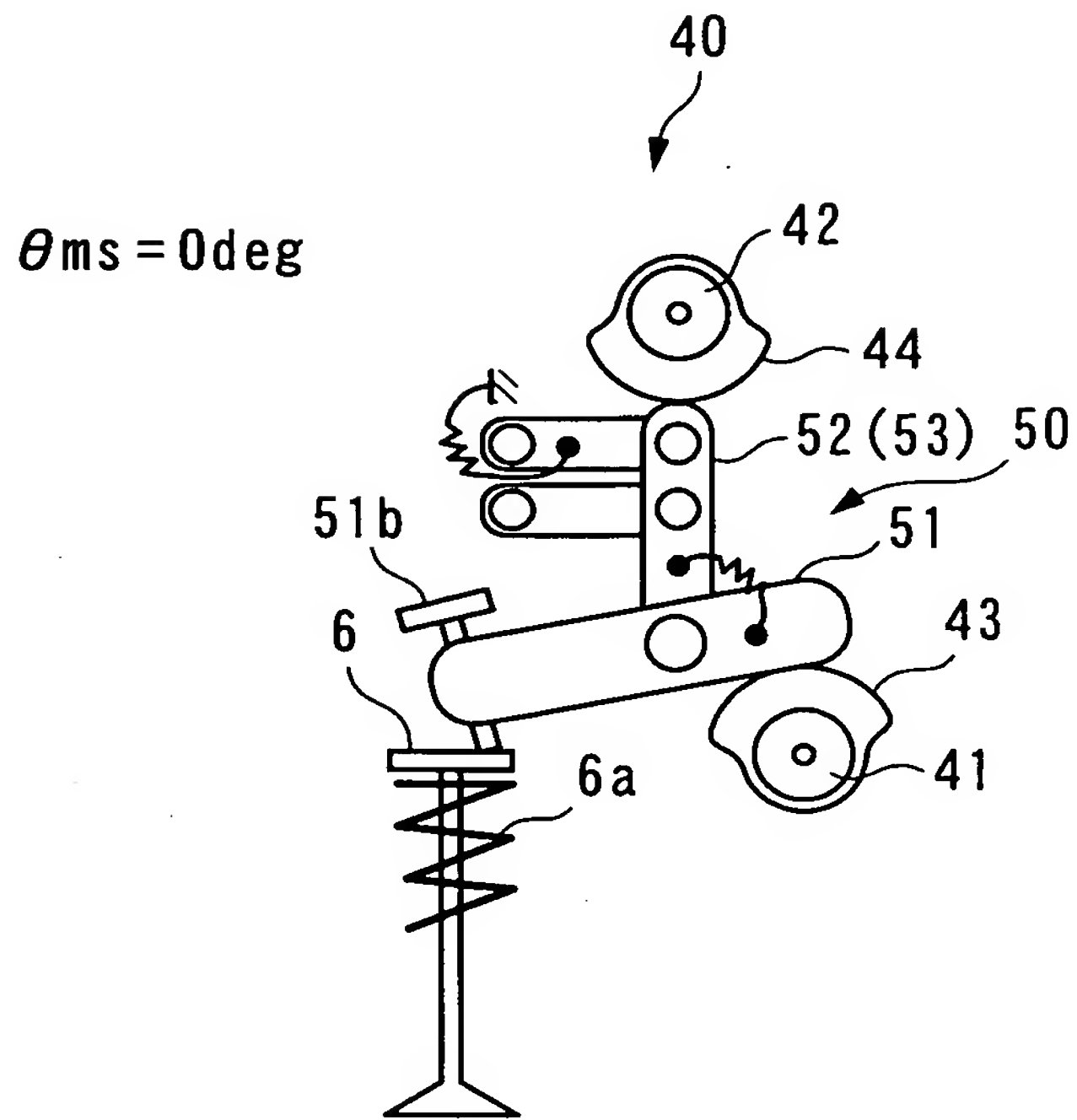


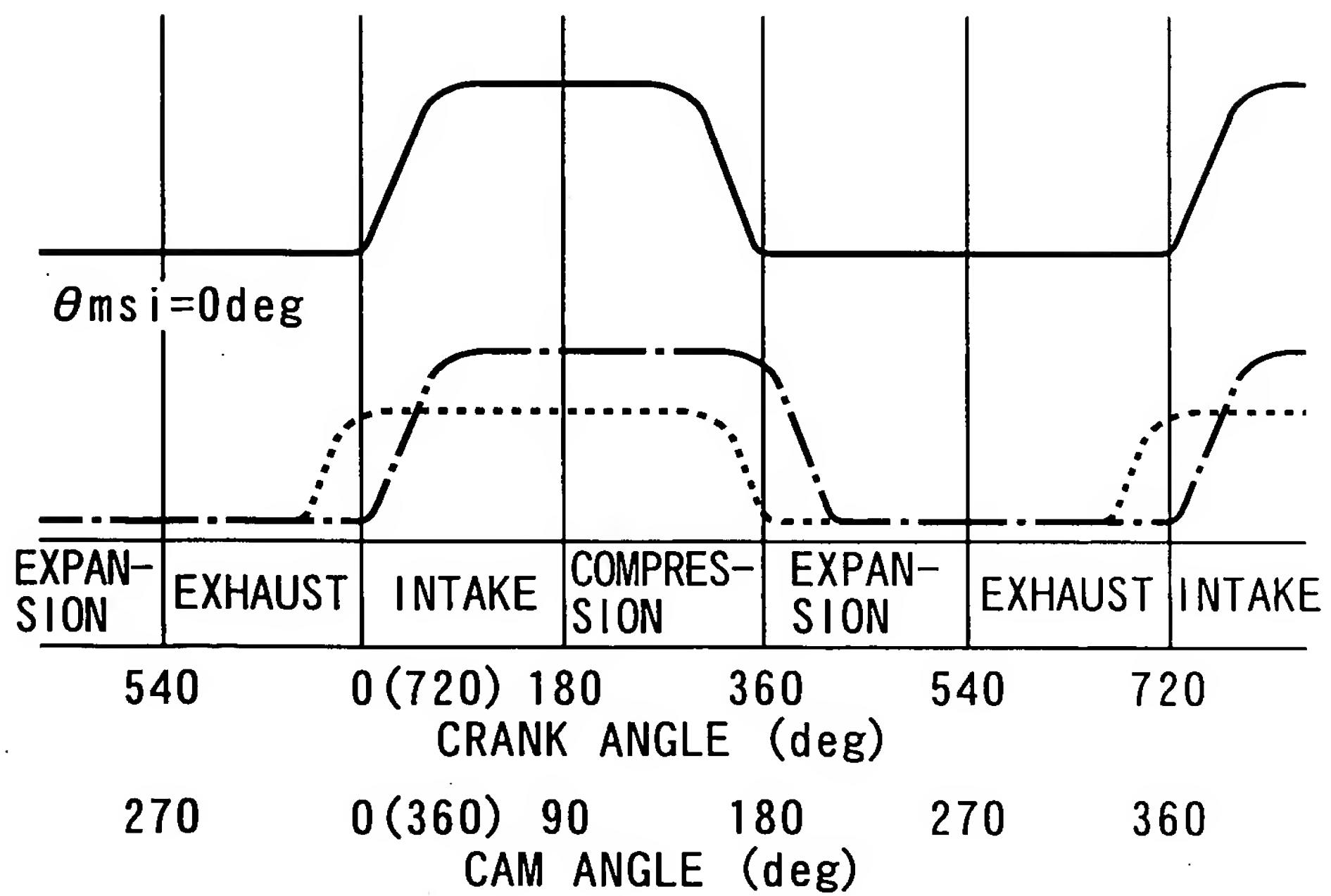
FIG. 11



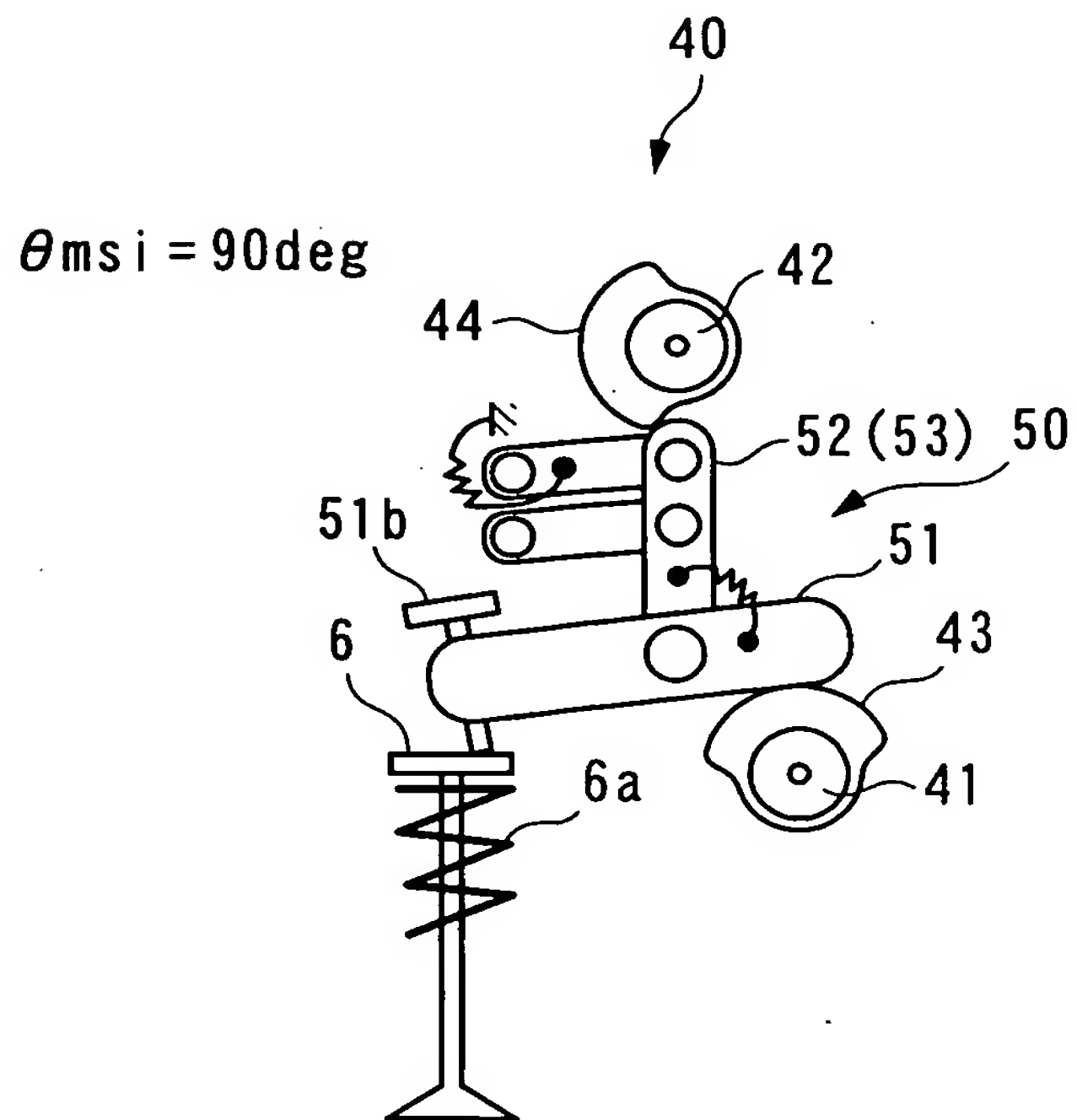
F I G. 1 2 A



F I G. 1 2 B



F I G. 1 3 A



F I G. 1 3 B

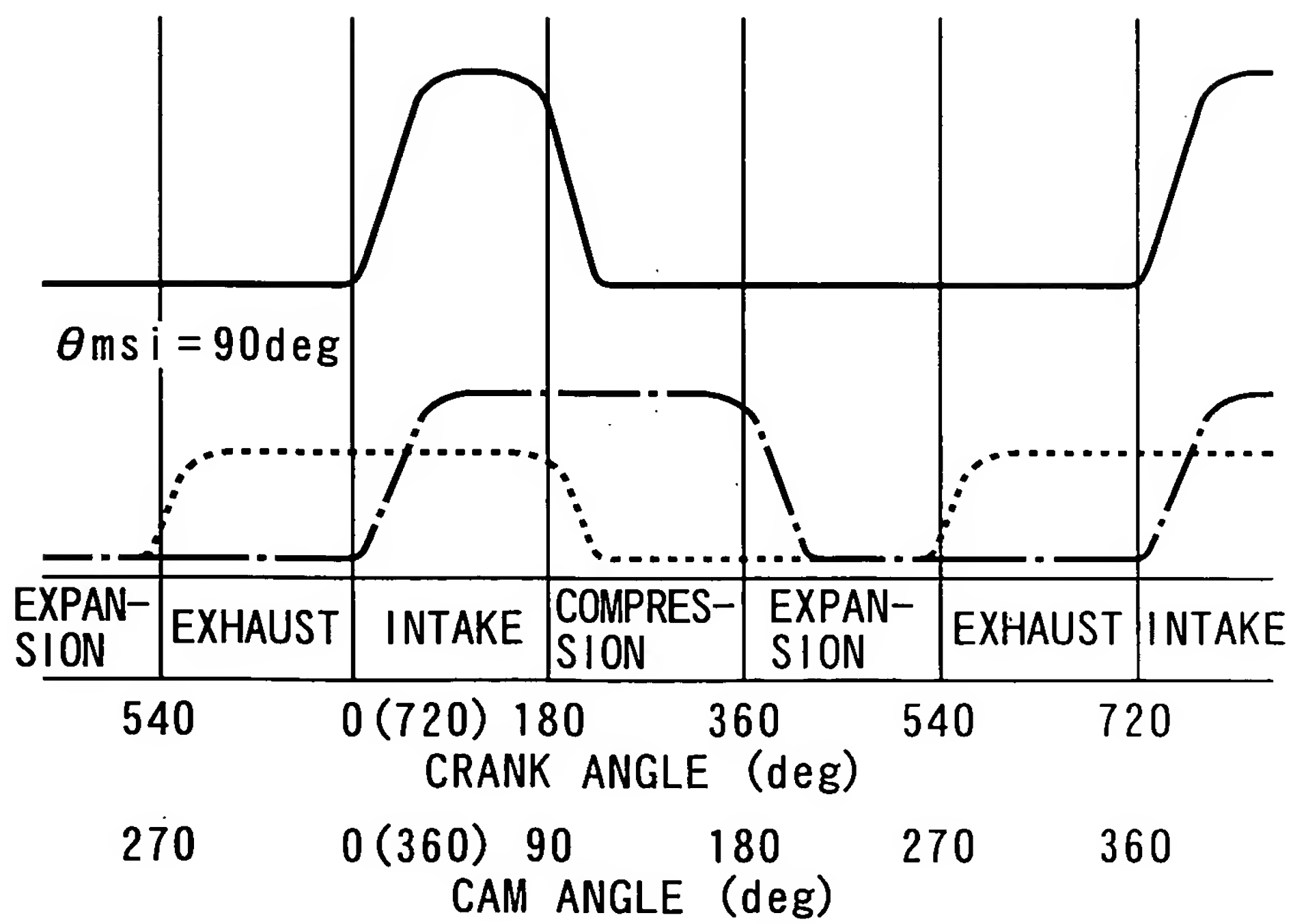
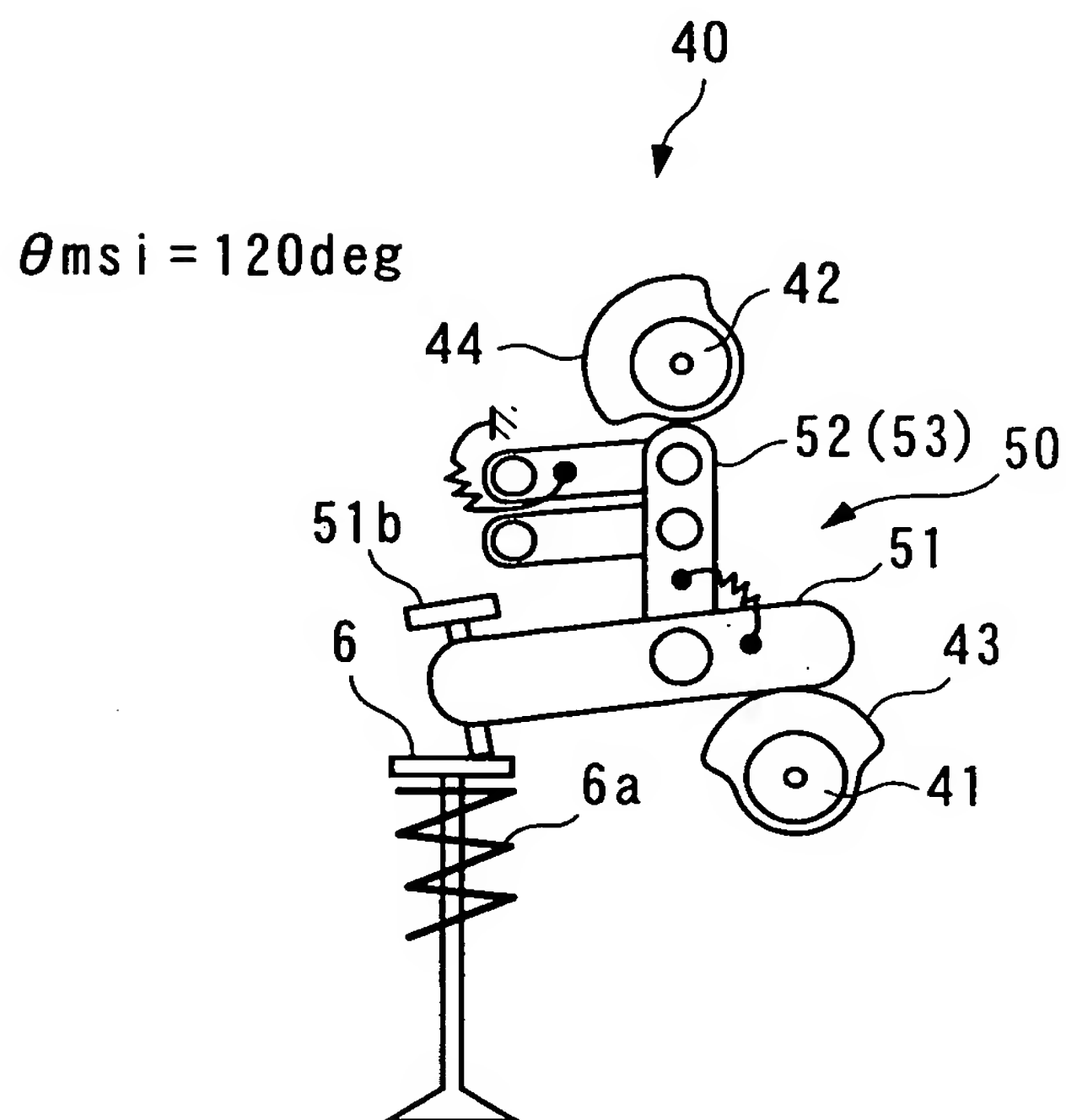
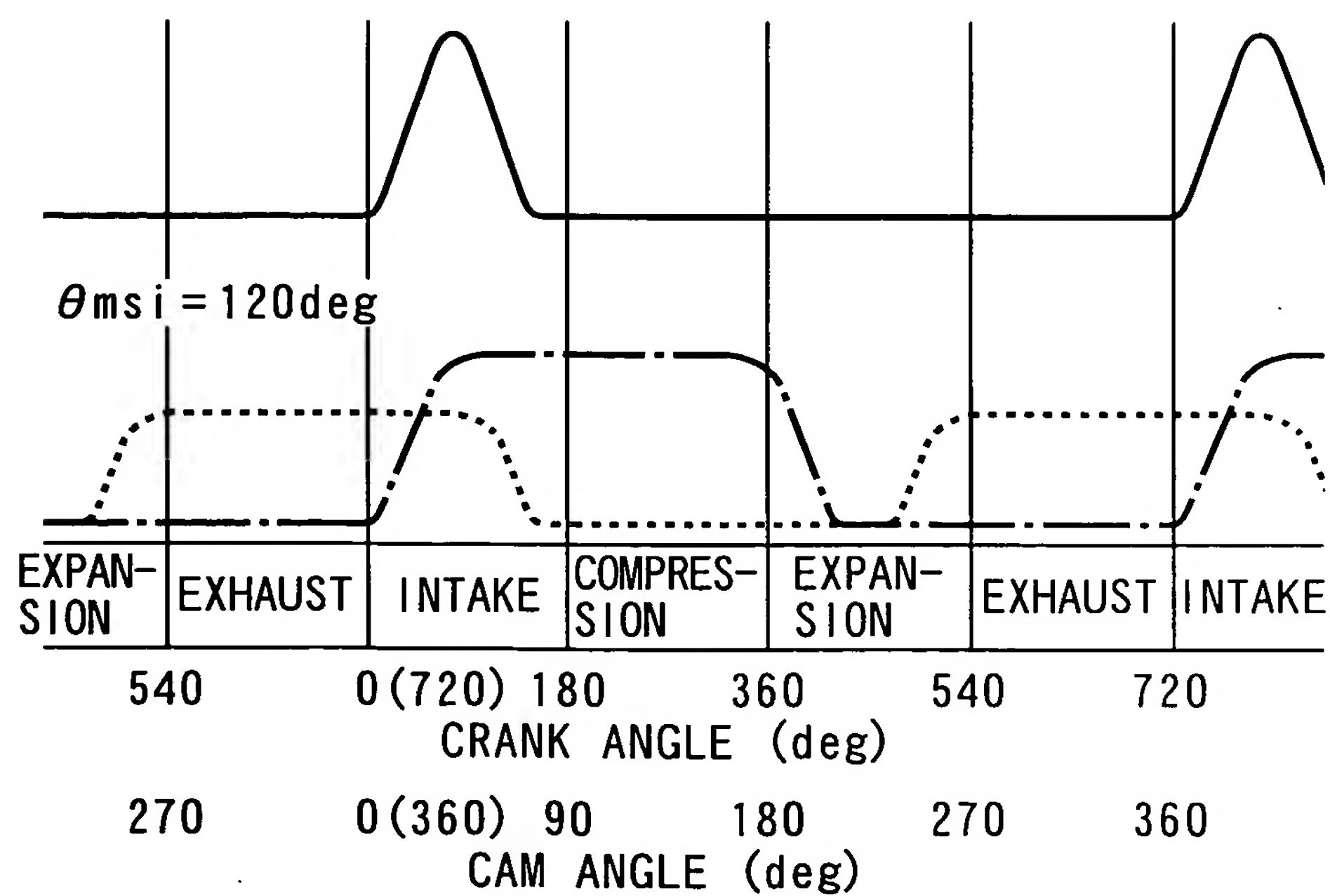


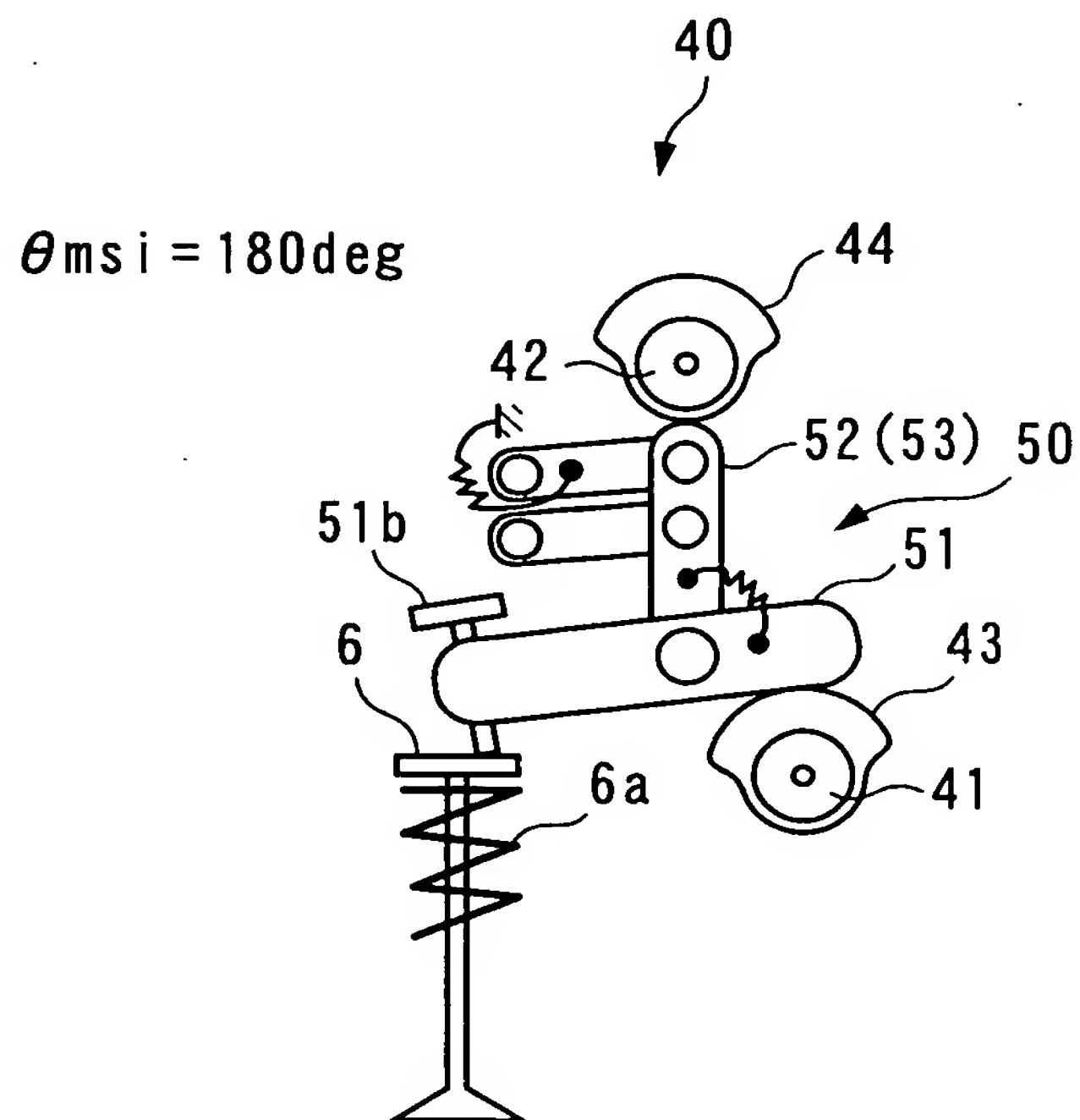
FIG. 14A



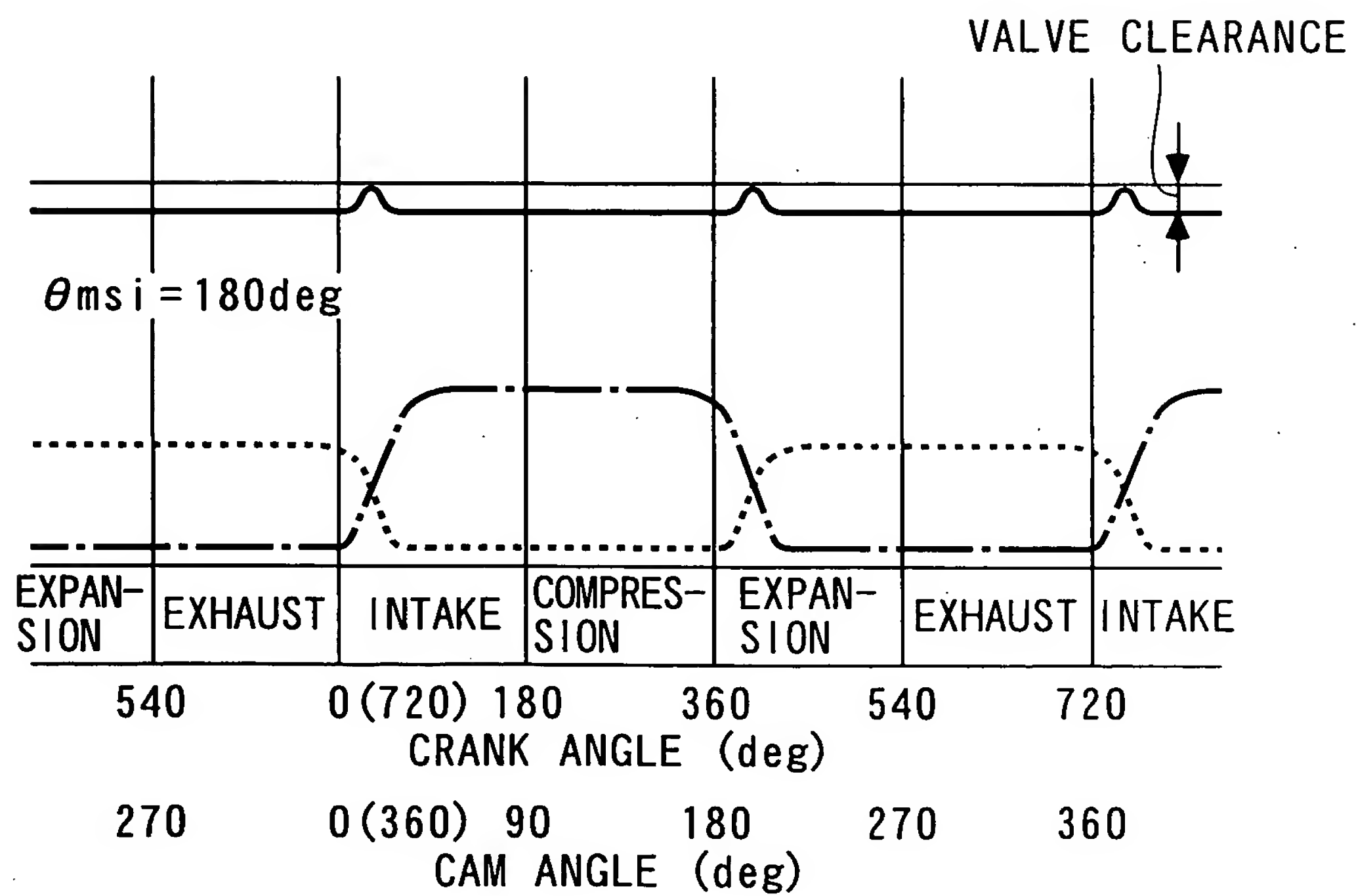
F I G. 1 4 B



F I G. 1 5 A



F I G. 1 5 B



F I G . 1 6

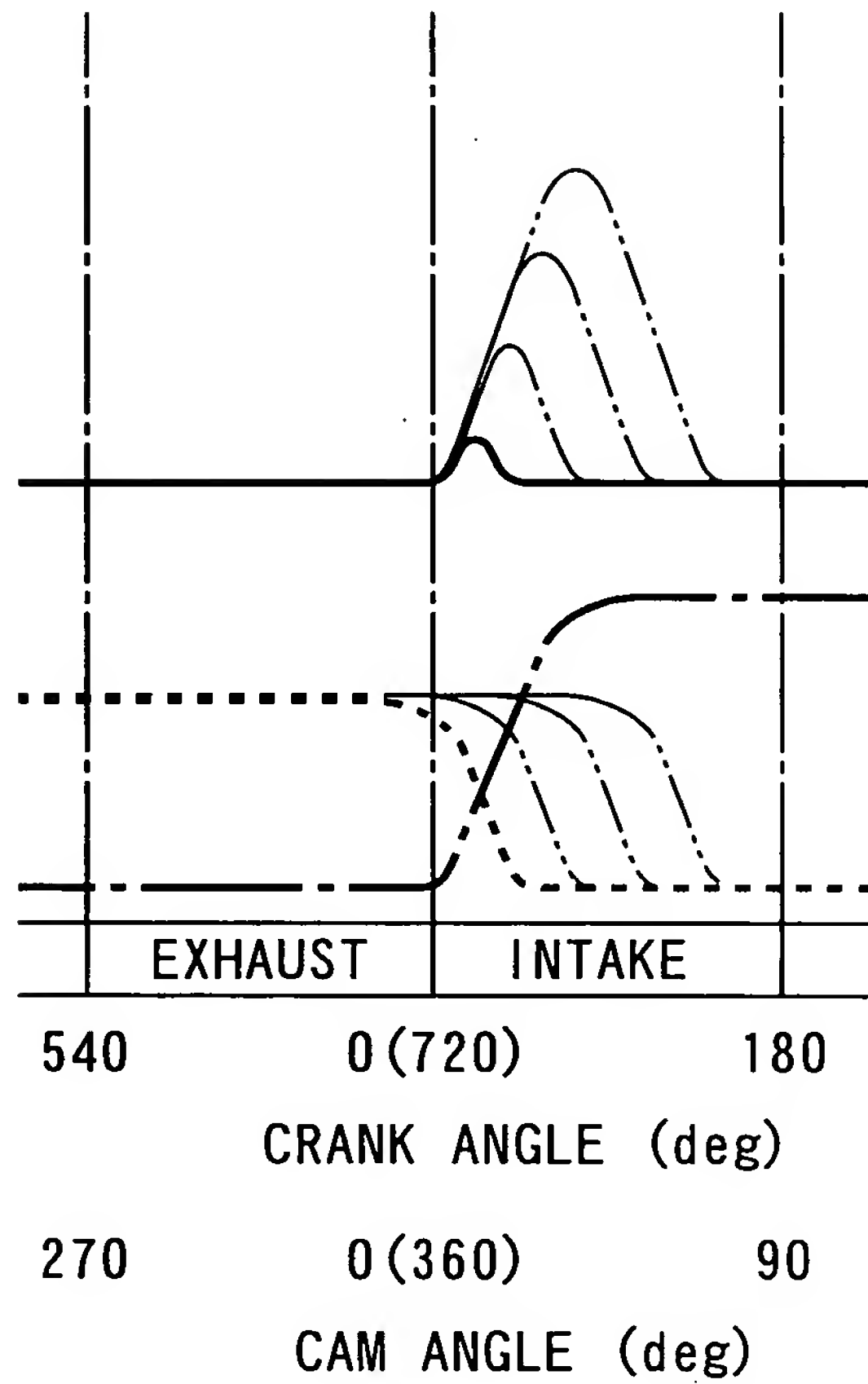
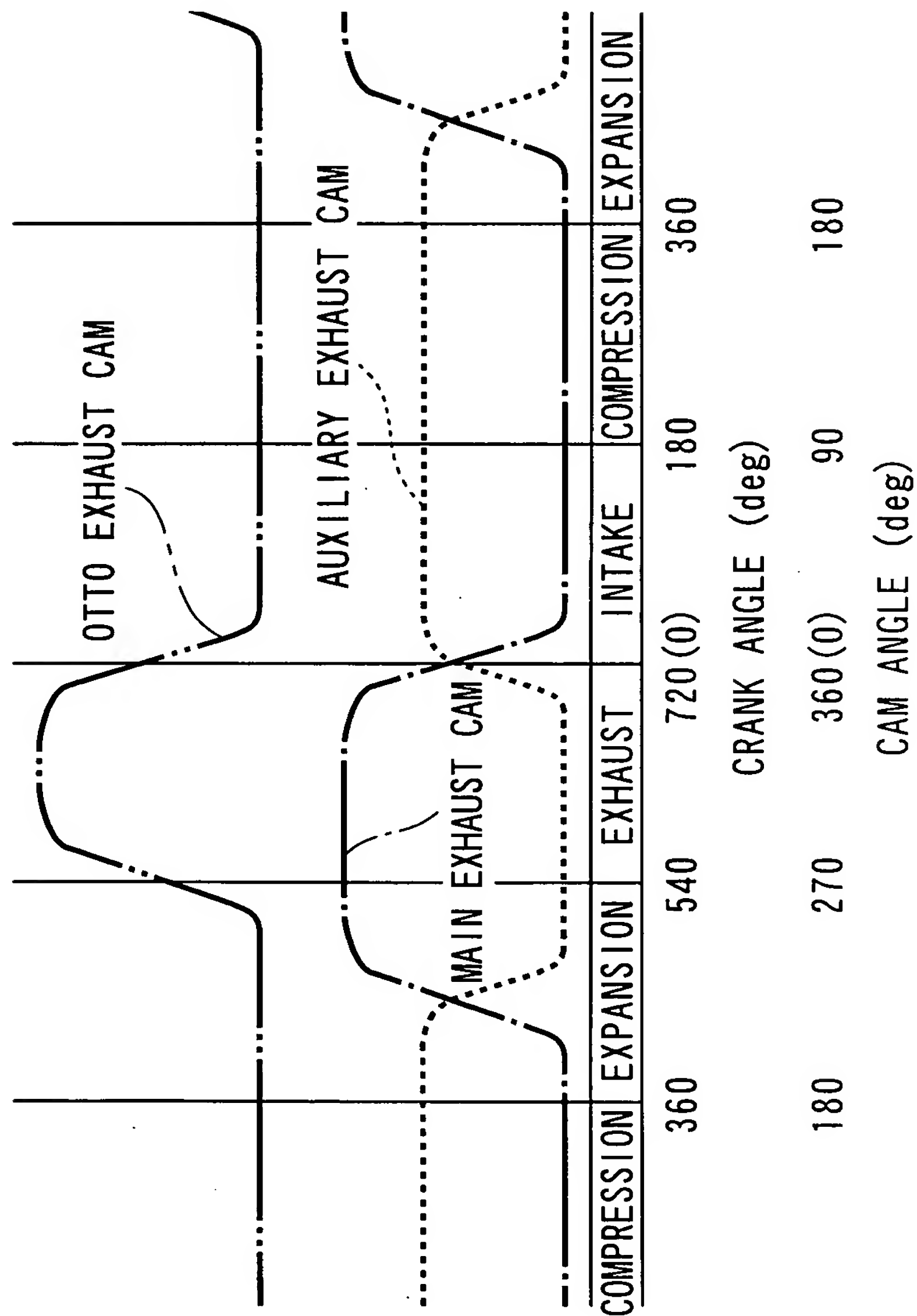
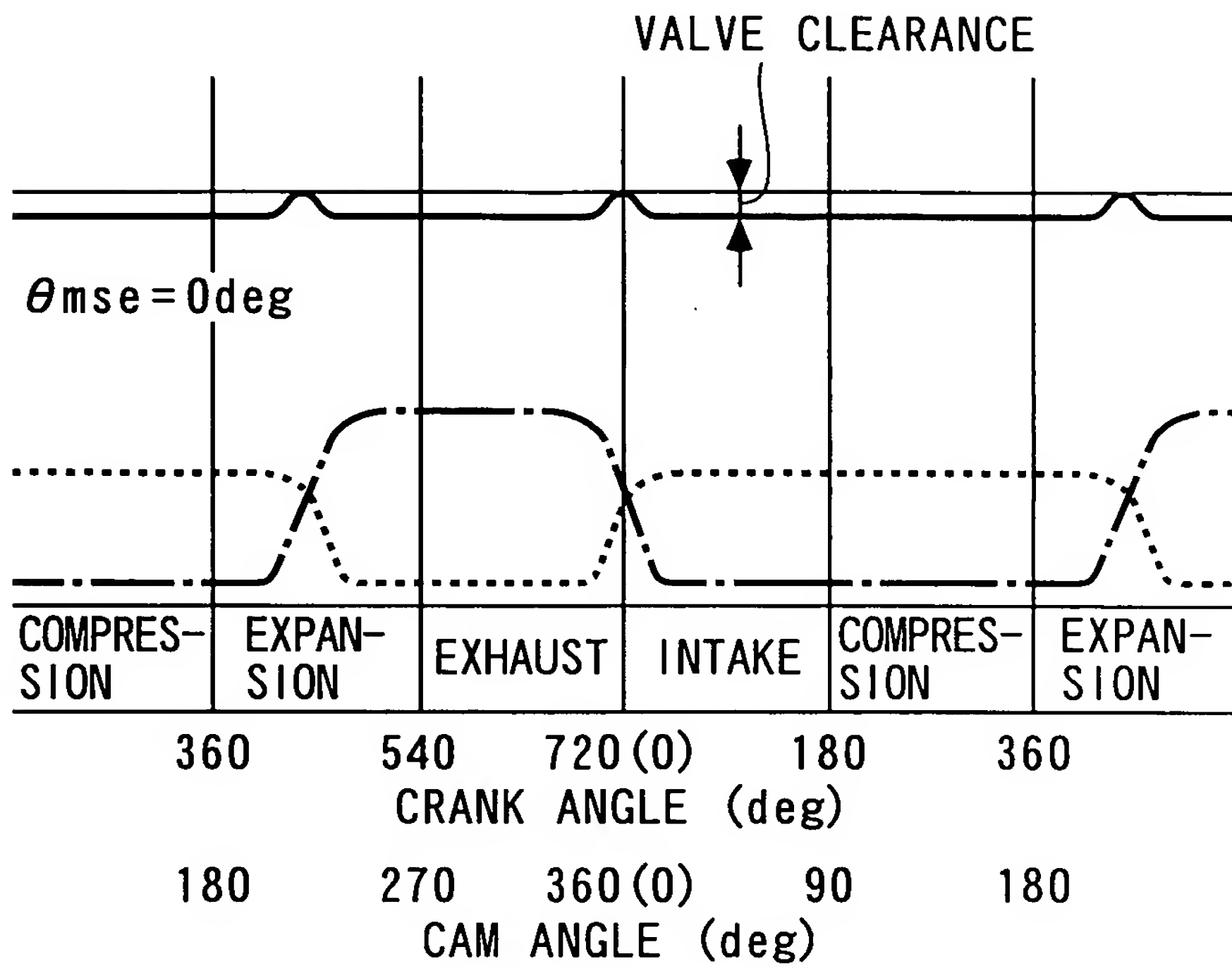




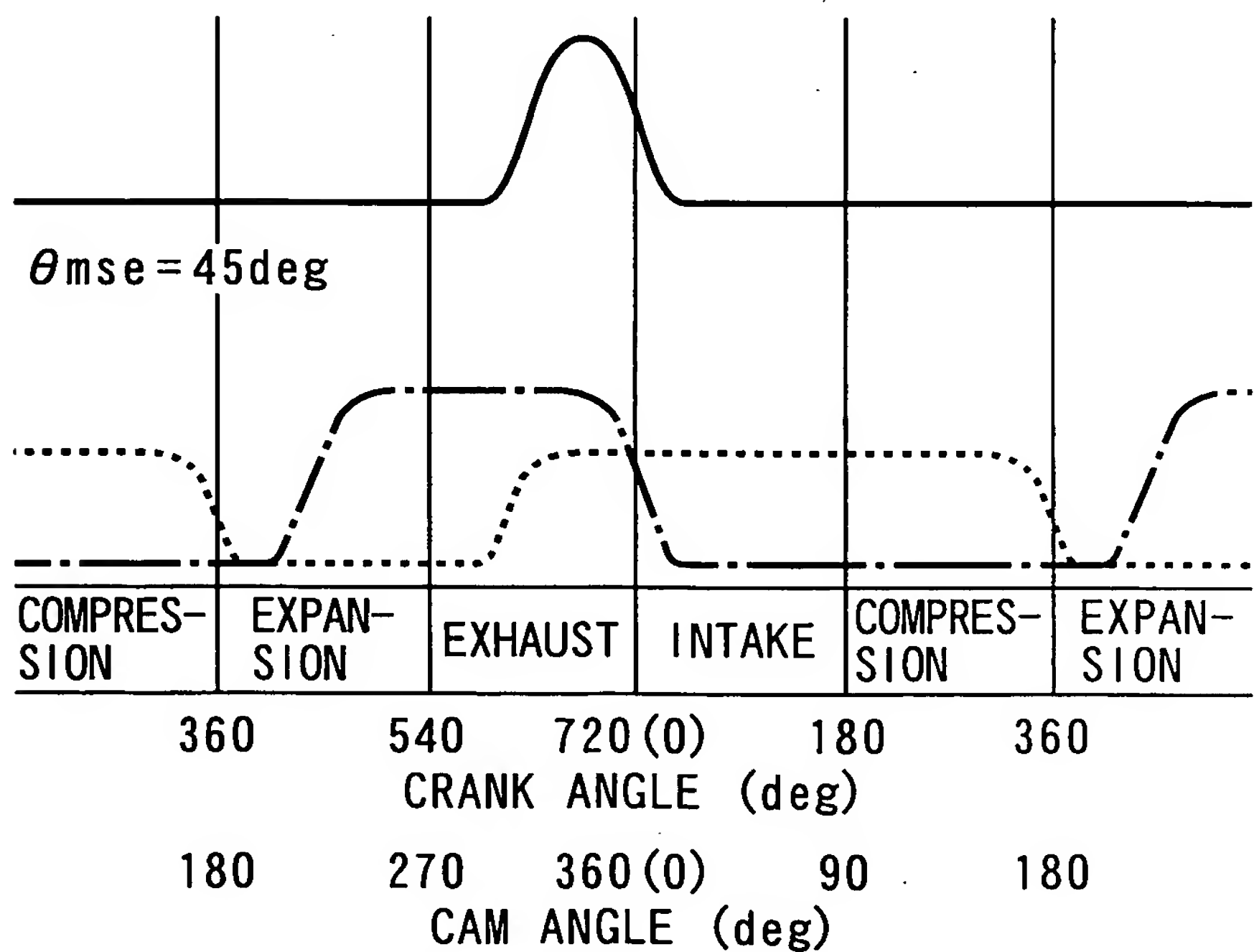
FIG. 17



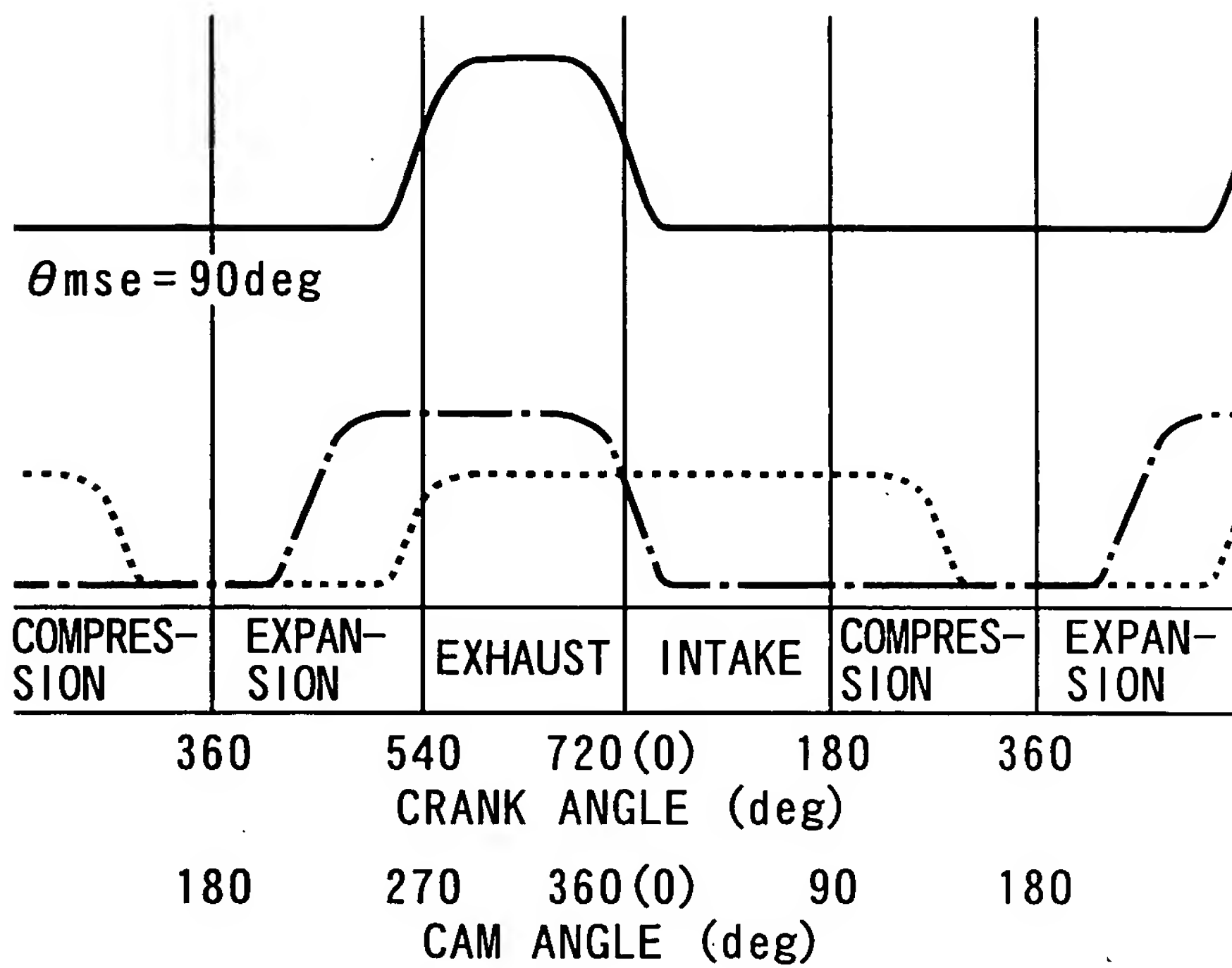
F I G. 1 8



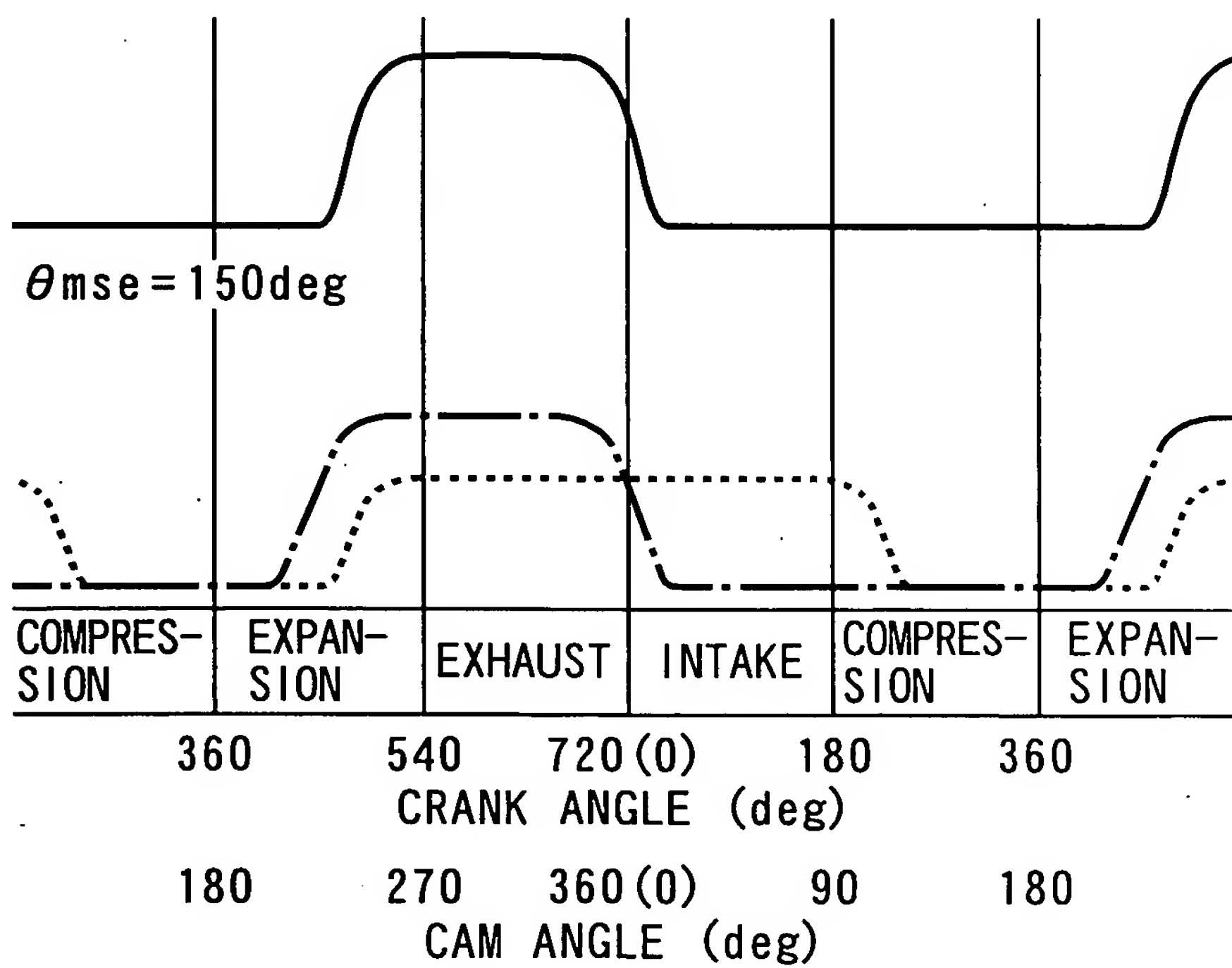
F I G. 1 9



F I G. 2 0



F I G. 2 1



F I G. 2 2

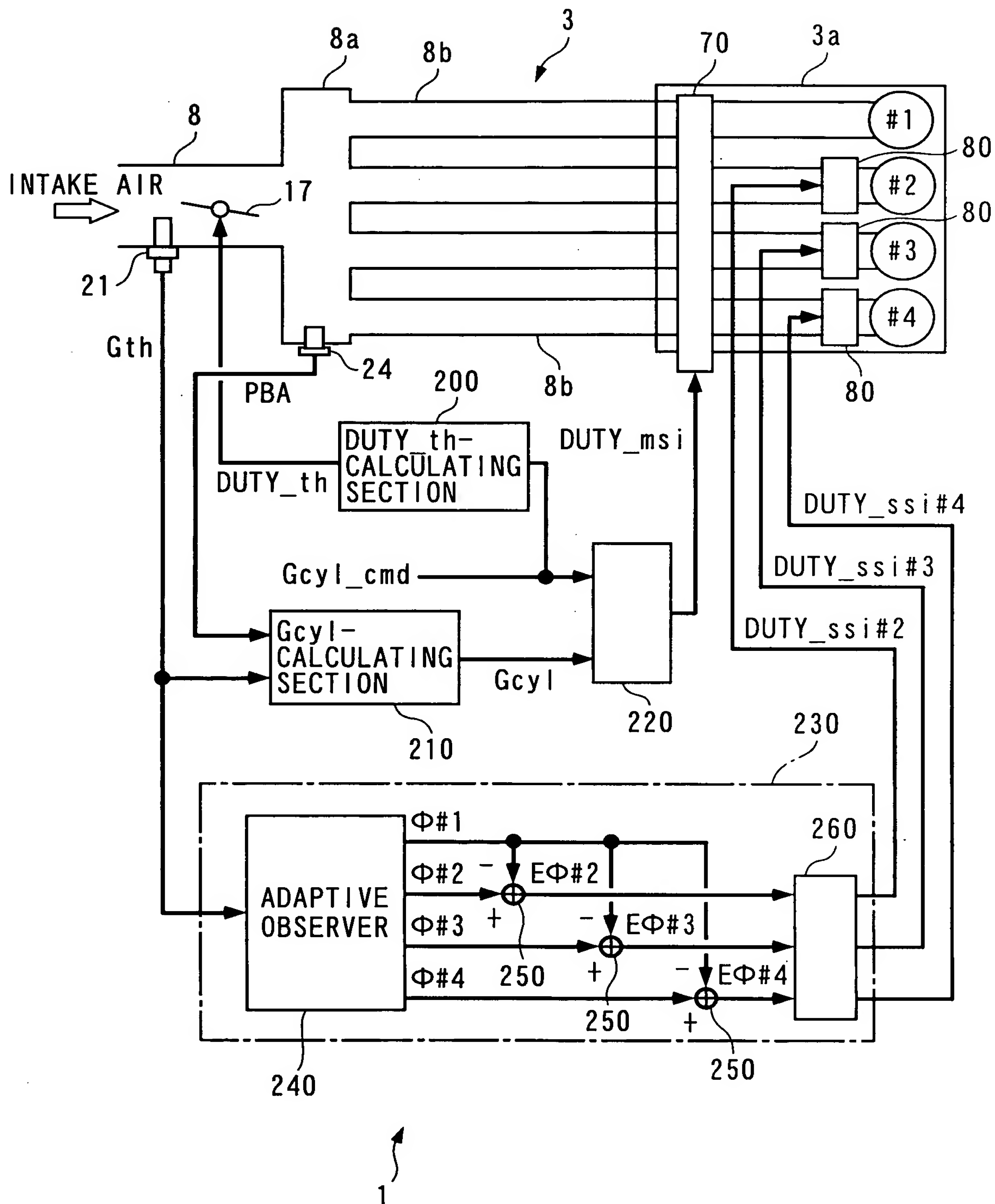
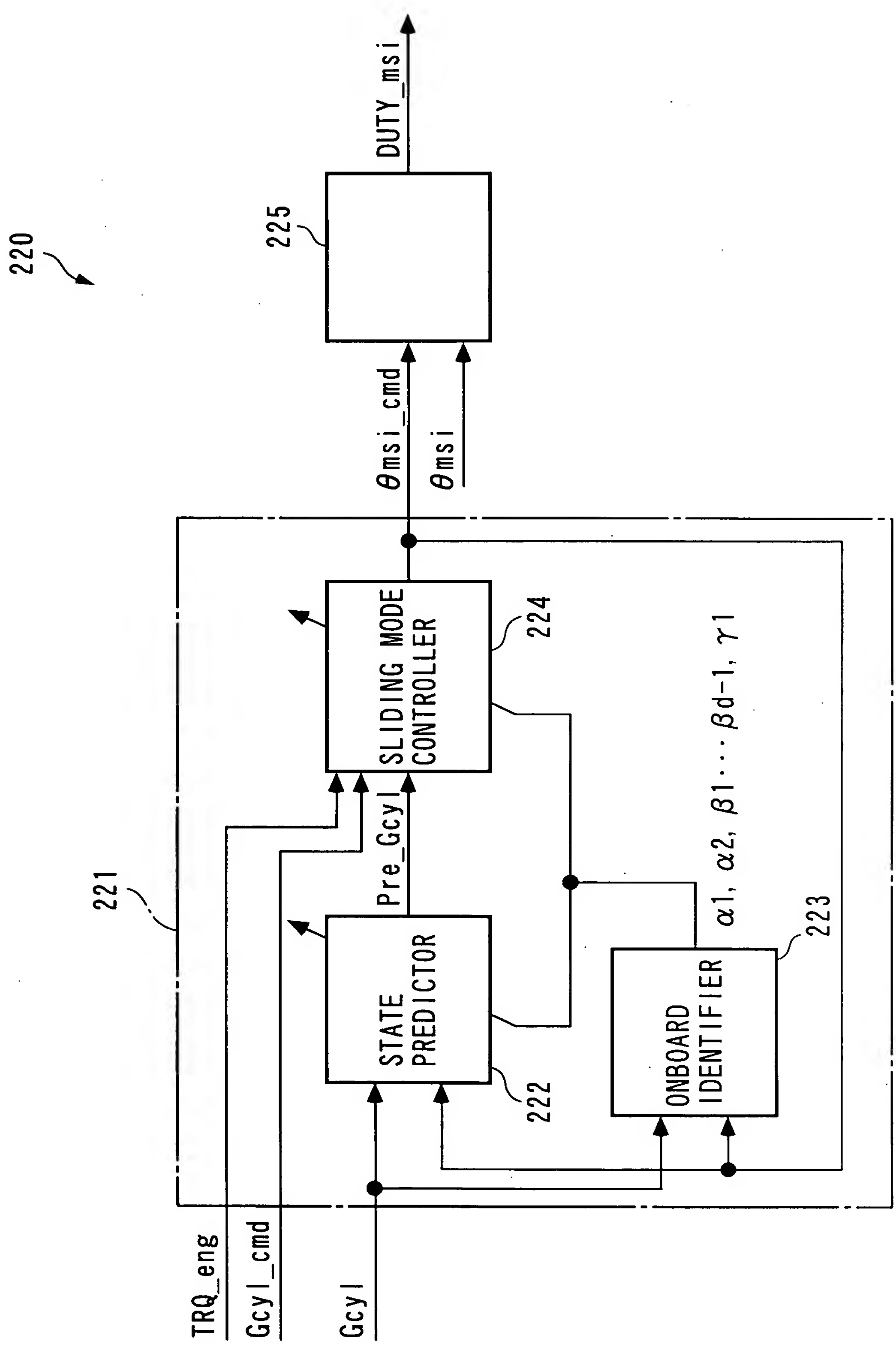


FIG. 23



## F I G. 2 4

$$G_{cyl}(n) = G_{th}(n) - \frac{VB \cdot [PBA(n) - PBA(n-1)]}{R \cdot TB} \quad \dots\dots (1)$$

$$G_{cyl}(n) = a1 \cdot G_{cyl}(n-1) + a2 \cdot G_{cyl}(n-2) + b1 \cdot \theta_{msi}(n-d) \quad \dots\dots (2)$$

$$G_{cyl}(n+d-1) = a1 \cdot G_{cyl}(n+d-2) + a2 \cdot G_{cyl}(n+d-3) + b1 \cdot \theta_{msi}(n-1) \quad \dots\dots (3)$$

$$A = \begin{bmatrix} a1 & a2 \\ 1 & 0 \end{bmatrix} \quad \dots\dots (4)$$

$$B = \begin{bmatrix} b1 \\ 0 \end{bmatrix} \quad \dots\dots (5)$$

$$\begin{aligned}
 G_{cyl}(n+d-1) = & \alpha1 \cdot G_{cyl}(n) + \alpha2 \cdot G_{cyl}(n-1) \\
 & + \beta1 \cdot \theta_{msi}(n-1) + \beta2 \cdot \theta_{msi}(n-2) \\
 & + \dots + \beta_{d-1} \cdot \theta_{msi}(n-d+1) \quad \dots\dots (6)
 \end{aligned}$$

$\alpha1$  : FIRST-ROW FIRST-COLUMN ELEMENT OF  $A^{d-1}$   
 $\alpha2$  : FIRST-ROW SECOND-COLUMN ELEMENT OF  $A^{d-1}$   
 $\beta_j$  : FIRST-ROW ELEMENT OF  $A^{j-1} B$  ( $j = 0 \sim d-1$ )

$$\begin{aligned}
 Pre\_G_{cyl}(n) = & \alpha1 \cdot G_{cyl}(n) + \alpha2 \cdot G_{cyl}(n-1) \\
 & + \beta1 \cdot \theta_{msi}(n-1) + \beta2 \cdot \theta_{msi}(n-2) \\
 & + \dots + \beta_{d-1} \cdot \theta_{msi}(n-d+1) + \gamma1 \\
 \doteq & G_{cyl}(n+d-1) \quad \dots\dots (7)
 \end{aligned}$$

## F I G. 2 5

$$\theta_s(n) = \theta_s(n-1) + K P_s(n) \cdot ide(n) \quad \dots\dots (8)$$

$$K P_s(n) = \frac{P_s(n) \cdot \zeta_s(n)}{1 + \zeta_s(n)^T \cdot P_s(n) \cdot \zeta_s(n)} \quad \dots\dots (9)$$

$$P_s(n+1) = \frac{1}{\lambda_1} \left[ I - \frac{\lambda_2 \cdot P_s(n) \cdot \zeta_s(n) \cdot \zeta_s(n)^T}{\lambda_1 + \lambda_2 \cdot \zeta_s(n)^T \cdot P_s(n) \cdot \zeta_s(n)} \right] P_s(n) \quad \dots\dots (10)$$

I : UNIT MATRIX OF ORDER  $d+2$   
 $\lambda_1, \lambda_2$  : WEIGHTING PARAMETER

$$\begin{aligned} ide(n) &= Pre\_Gcyl(n-d+1) - Gcyl(n) \\ &= \theta_s(n-1)^T \cdot \zeta_s(n) - Gcyl(n) \end{aligned} \quad \dots\dots (11)$$

$$\theta_s(n)^T = [\alpha_1, \alpha_2, \beta_1, \beta_2, \dots, \beta_{d-1}, \gamma_1] \quad \dots\dots (12)$$

$$\begin{aligned} \zeta_s(n)^T &= [Gcyl(n-d), Gcyl(n-d-1), \\ &\quad \theta_{msi}(n-d), \theta_{msi}(n-d-1), \dots, \theta_{msi}(n-2d+2), 1] \end{aligned} \quad \dots\dots (13)$$

## F I G. 2 6

$$\begin{aligned}
 Gcyl(n+d) = & \alpha 1 \cdot Gcyl(n+1) + \alpha 2 \cdot Gcyl(n) \\
 & + \beta 1 \cdot \theta msi(n) + \beta 2 \cdot \theta msi(n-1) \\
 & + \dots + \beta d-1 \cdot \theta msi(n-d+2) + \gamma 1 \quad \dots\dots (14)
 \end{aligned}$$

$$Es(n) = Gcyl(n) - Gcyl\_cmd(n) \quad \dots\dots (15)$$

$$\sigma s(n) = Es(n) + Ss \cdot Es(n-1) \quad \dots\dots (16)$$

$$-1 < Ss < 0 \quad \dots\dots (17)$$

$$\begin{aligned}
 \theta msi\_cmd(n) &= Uspas(n) \\
 &= Ueq(n) + Urch(n) + Uvt(n) \quad \dots\dots (18)
 \end{aligned}$$

$$\begin{aligned}
 Ueq(n) = & \frac{1}{\beta 1} \{ Pre\_Gcyl(n) + Ss \cdot Pre\_Gcyl(n-1) \\
 & - \alpha 1 \cdot Pre\_Gcyl(n-d+1) - \alpha 2 \cdot Gcyl(n) \\
 & - \beta 2 \cdot \theta msi(n-1) - \dots - \beta d-1 \cdot \theta msi(n-d+2) - \gamma 1 \\
 & + Gcyl\_cmd(n+d) + (Ss-1) \cdot Gcyl\_cmd(n+d-1) \\
 & - Ss \cdot Gcyl\_cmd(n+d-2) \} \quad \dots\dots (19)
 \end{aligned}$$

$$Urch(n) = \frac{-F}{\beta 1} \cdot \sigma s(n+d-1) \quad \dots\dots (20)$$

F : REACHING LAW GAIN (0 < F < 2)

$$Uvt(n) = \theta msi\_base(n) \quad \dots\dots (21)$$



## F I G. 2 7

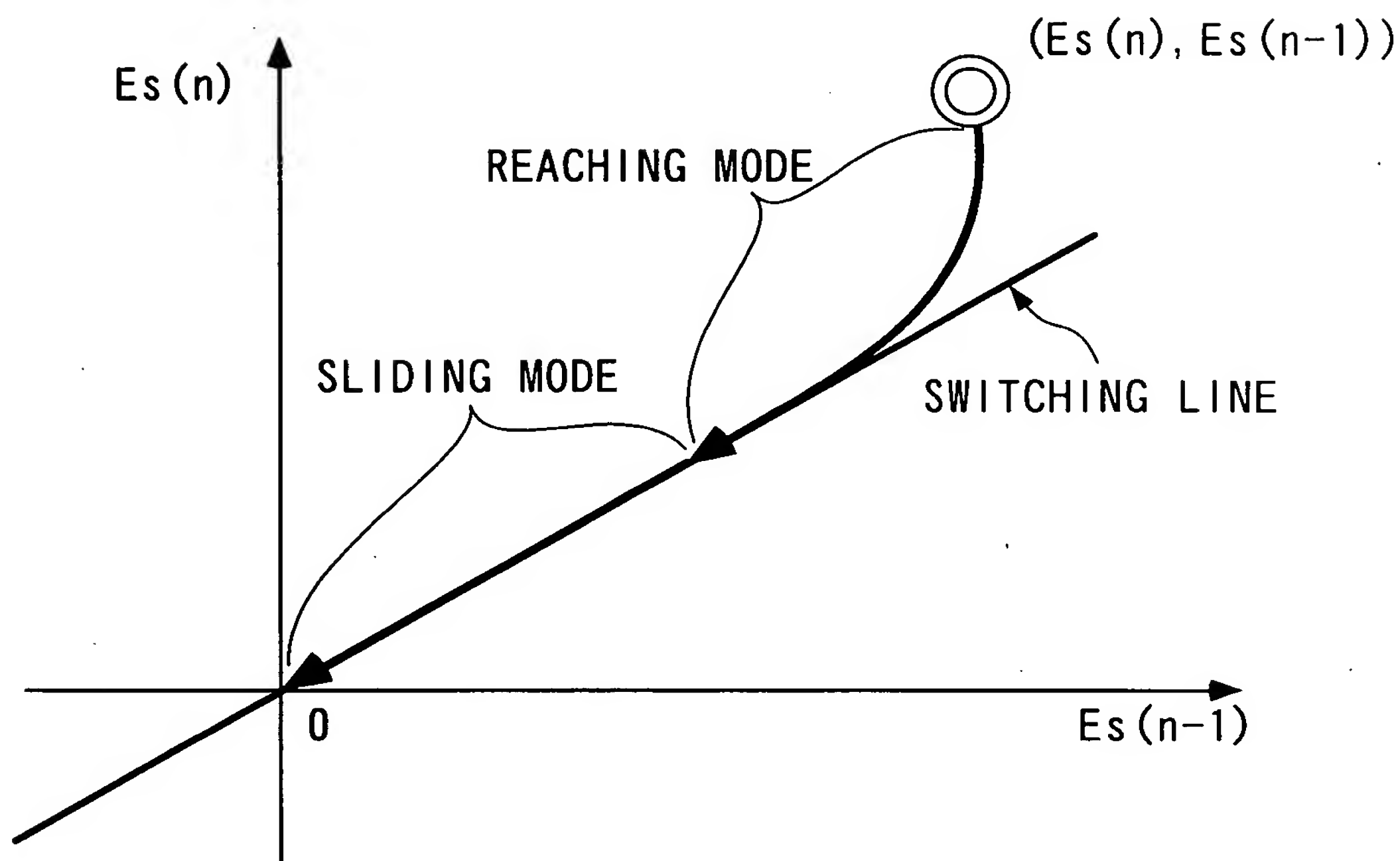
$$\sigma s(n+d) = \sigma s(n+d-1) \quad \dots\dots (22)$$

$$E s(n+d) + S s \cdot E s(n+d-1) = E s(n+d-1) + S s \cdot E s(n+d-2) \quad \dots\dots (23)$$

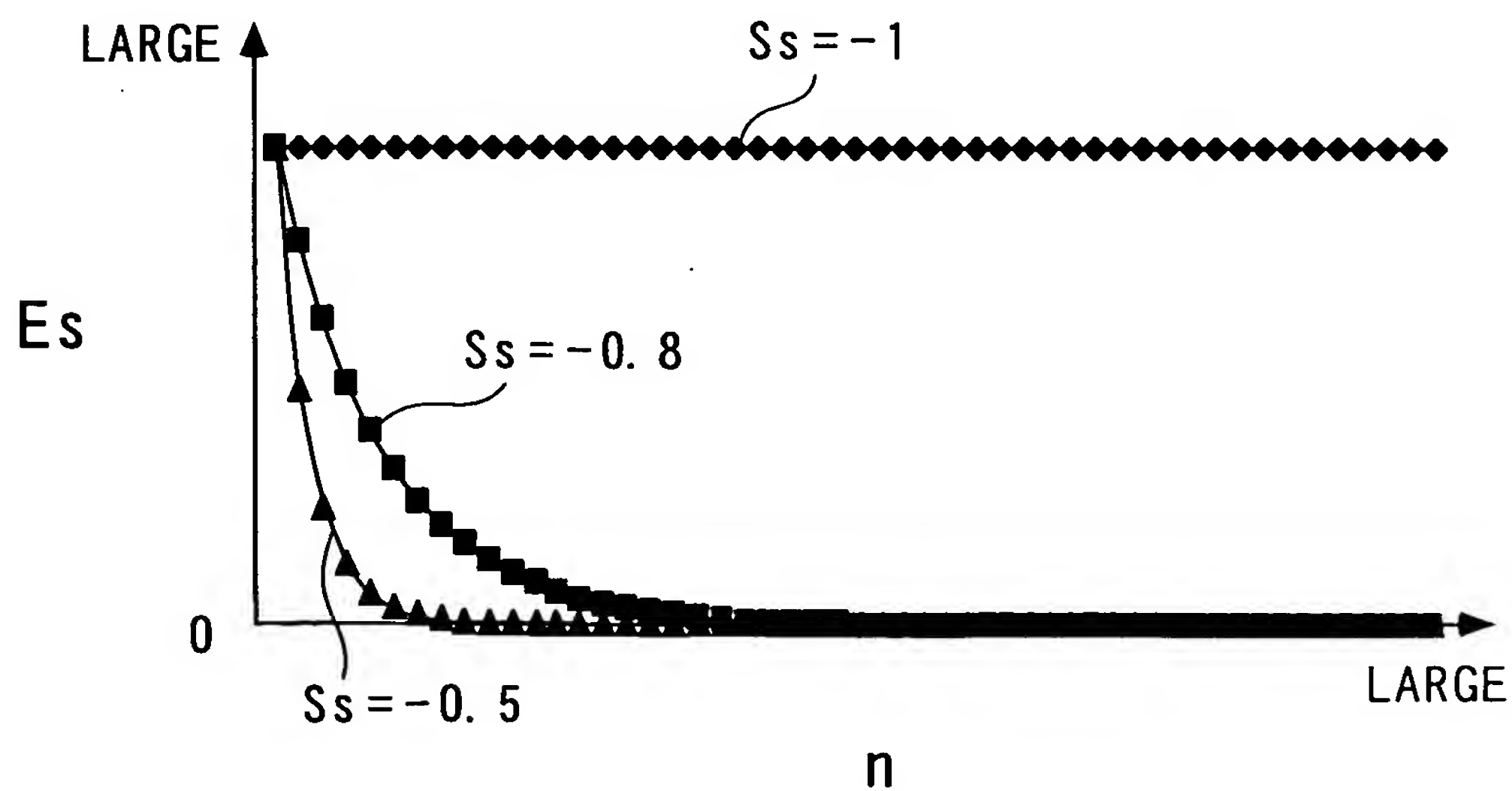
$$\begin{aligned} & \alpha 1 \cdot G c y l(n+1) + \alpha 2 \cdot G c y l(n) + \beta 1 \cdot \theta m s i(n) + \beta 2 \cdot \theta m s i(n-1) \\ & + \dots + \beta d-1 \cdot \theta m s i(n-d+2) + \gamma 1 - G c y l\_c m d(n+d) \\ & + S s \cdot G c y l(n+d-1) - S s \cdot G c y l\_c m d(n+d-1) \\ & = G c y l(n+d-1) - G c y l\_c m d(n+d-1) \\ & + S s \cdot G c y l(n+d-2) - S s \cdot G c y l\_c m d(n+d-2) \quad \dots\dots (24) \end{aligned}$$

$$\begin{aligned} \theta m s i(n) = \frac{1}{\beta 1} \{ & G c y l(n+d-1) + S s \cdot G c y l(n+d-2) \\ & - \alpha 1 \cdot G c y l(n+1) - \alpha 2 \cdot G c y l(n) \\ & - \beta 2 \cdot \theta m s i(n-1) - \dots - \beta d-1 \cdot \theta m s i(n-d+2) - \gamma 1 \\ & + G c y l\_c m d(n+d) + (S s - 1) \cdot G c y l\_c m d(n+d-1) \\ & - S s \cdot G c y l\_c m d(n+d-2) \} \quad \dots\dots (25) \end{aligned}$$

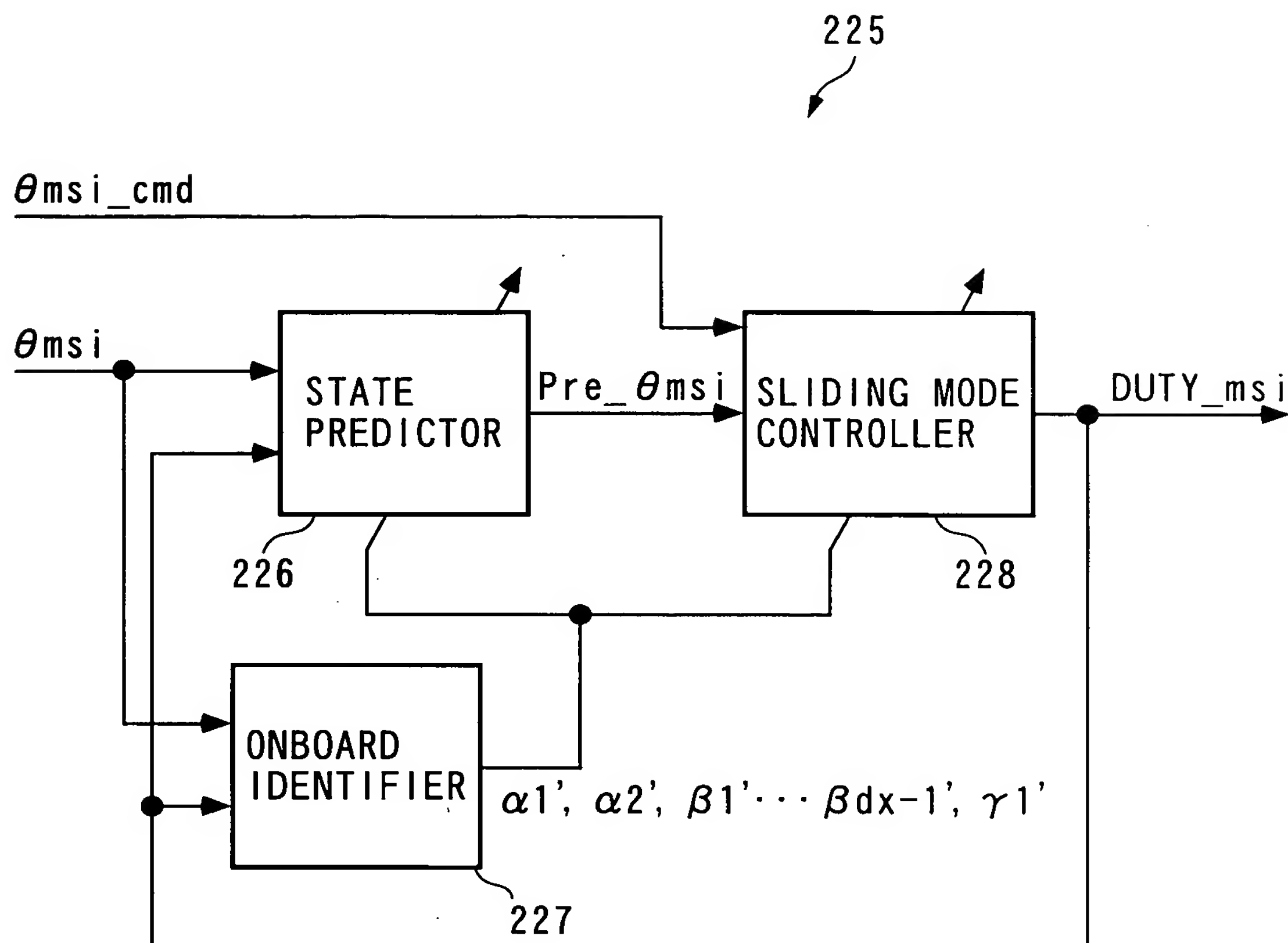
F I G. 2 8



F I G. 2 9



F I G . 3 0



## F I G. 3 1

$$\theta_{msi}(m) = a1' \cdot \theta_{msi}(m-1) + a2' \cdot \theta_{msi}(m-2) + b1' \cdot DUTY_{msi}(m-dx) \quad \dots\dots (26)$$

$$A' = \begin{bmatrix} a1' & a2' \\ 1 & 0 \end{bmatrix} \quad \dots\dots (27)$$

$$B' = \begin{bmatrix} b1' \\ 0 \end{bmatrix} \quad \dots\dots (28)$$

$$\begin{aligned} Pre\_ \theta_{msi}(m) &= \alpha1' \cdot \theta_{msi}(m) + \alpha2' \cdot \theta_{msi}(m-1) \\ &\quad + \beta1' \cdot DUTY_{msi}(m-1) + \beta2' \cdot DUTY_{msi}(m-2) \\ &\quad + \dots + \beta_{dx-1}' \cdot DUTY_{msi}(m-dx+1) + \gamma1' \\ &\doteq \theta_{msi}(m+dx-1) \quad \dots\dots (29) \end{aligned}$$

$\alpha1'$  : FIRST-ROW FIRST-COLUMN ELEMENT OF  $A'^{dx-1}$   
 $\alpha2'$  : FIRST-ROW SECOND-COLUMN ELEMENT OF  $A'^{dx-1}$   
 $\beta_j'$  : FIRST-ROW ELEMENT OF  $A'^{j'-1} B'$  ( $j' = 0 \sim dx-1$ )

## F I G. 3 2

$$\theta s'(m) = \theta s'(m-1) + KPs'(m) \cdot ide'(m) \quad \dots\dots (30)$$

$$KPs'(m) = \frac{Ps'(m) \cdot \zeta s'(m)}{1 + \zeta s'(m)^T \cdot Ps'(m) \cdot \zeta s'(m)} \quad \dots\dots (31)$$

$$Ps'(m+1) = \frac{1}{\lambda 1'} \left[ I' - \frac{\lambda 2' \cdot Ps'(m) \cdot \zeta s'(m) \cdot \zeta s'(m)^T}{\lambda 1' + \lambda 2' \cdot \zeta s'(m)^T \cdot Ps'(m) \cdot \zeta s'(m)} \right] Ps'(m) \quad \dots\dots (32)$$

$I'$ : UNIT MATRIX OF ORDER  $dx+2$   
 $\lambda 1', \lambda 2'$ : WEIGHTING PARAMETER

$$\begin{aligned} ide'(m) &= Pre\_ \theta msi(m-dx+1) - \theta msi(m) \\ &= \theta s'(m-1)^T \cdot \zeta s'(m) - \theta msi(m) \end{aligned} \quad \dots\dots (33)$$

$$\theta s'(m)^T = [\alpha 1', \alpha 2', \beta 1', \beta 2', \dots, \beta dx-1', \gamma 1'] \quad \dots\dots (34)$$

$$\begin{aligned} \zeta s'(m)^T &= [\theta msi(m-dx), \theta msi(m-dx-1), \\ &\quad DUTY\_msi(m-dx), DUTY\_msi(m-dx-1), \dots \\ &\quad \dots, DUTY\_msi(m-2dx+2), 1] \end{aligned} \quad \dots\dots (35)$$

## F I G. 3 3

$$Es'(m) = \theta_{msi}(m) - \theta_{msi\_cmd}(m) \quad \dots\dots (36)$$

$$\sigma s'(m) = Es'(m) + Ss' \cdot Es'(m-1) \quad \dots\dots (37)$$

$$-1 < Ss' < 0 \quad \dots\dots (38)$$

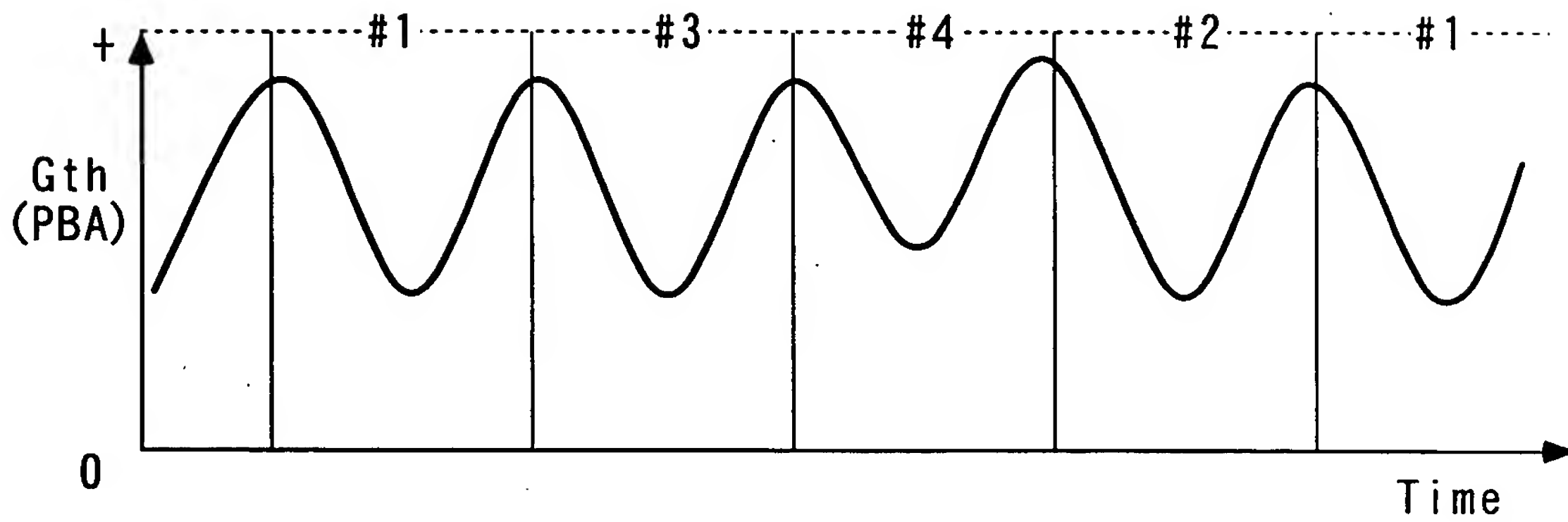
$$DUTY_{msi}(m) = U_{spas'}(m) = U_{eq'}(m) + U_{rch'}(m) \quad \dots\dots (39)$$

$$\begin{aligned}
 U_{eq'}(m) = & \frac{1}{\beta 1'} \{ Pre\_ \theta_{msi}(m) + Ss' \cdot Pre\_ \theta_{msi}(m-1) \\
 & - \alpha 1' \cdot Pre\_ \theta_{msi}(m-dx+1) - \alpha 2' \cdot \theta_{msi}(m) \\
 & - \beta 2' \cdot DUTY_{msi}(m-1) - \dots - \beta_{dx-1}' \cdot DUTY_{msi}(m-dx+2) - \gamma 1' \\
 & + \theta_{msi\_cmd}(m+dx) + (Ss'-1) \cdot \theta_{msi\_cmd}(m+dx-1) \\
 & - Ss' \cdot \theta_{msi\_cmd}(m+dx-2) \} \quad \dots\dots (40)
 \end{aligned}$$

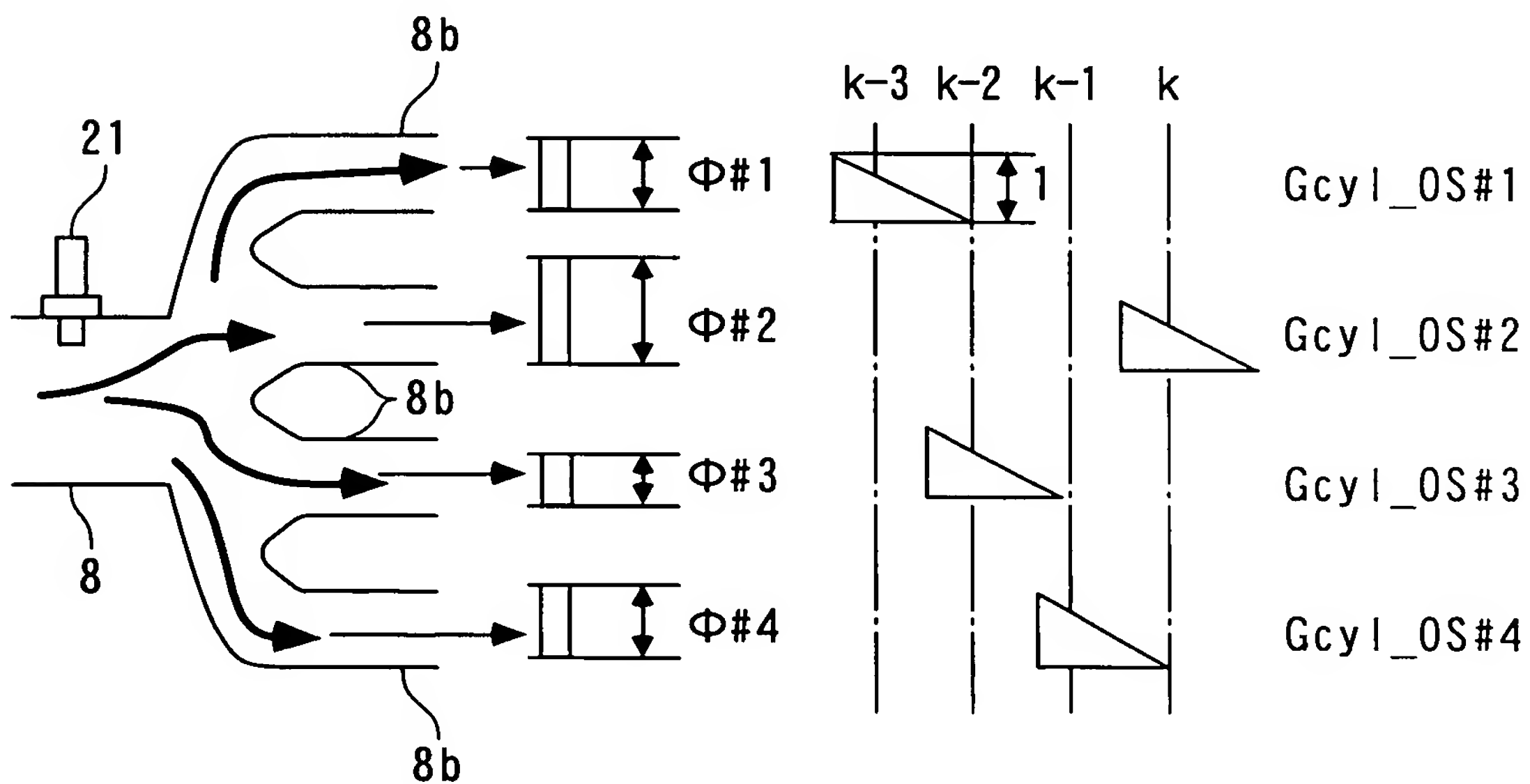
$$U_{rch'}(n) = \frac{-F'}{\beta 1'} \cdot \sigma s'(m+dx-1) \quad \dots\dots (41)$$

F' : REACHING LAW GAIN ( $0 < F' < 2$ )

F I G. 3 4



F I G. 3 5



## F I G . 3 6

$$G_{th}(k-d') = \Phi\#1(k) \cdot G_{cyl\_OS\#1}(k) + \Phi\#2(k) \cdot G_{cyl\_OS\#2}(k) \\ + \Phi\#3(k) \cdot G_{cyl\_OS\#3}(k) + \Phi\#4(k) \cdot G_{cyl\_OS\#4}(k) \\ \dots\dots (42)$$

$$G_{th\_est}(k) = \Phi\#1(k) \cdot G_{cyl\_OS\#1}(k) + \Phi\#2(k) \cdot G_{cyl\_OS\#2}(k) \\ + \Phi\#3(k) \cdot G_{cyl\_OS\#3}(k) + \Phi\#4(k) \cdot G_{cyl\_OS\#4}(k) \\ \dots\dots (43)$$

$$\phi(k) = \phi(k-1) + KR(k) \cdot ide'(k) \dots\dots (44)$$

$$KR(k) = \frac{R(k) \cdot \zeta'(k)}{1 + \zeta'(k)^T \cdot R(k) \cdot \zeta'(k)} \dots\dots (45)$$

$$ide'(k) = G_{th}(k-d') - G_{th\_est}(k) \dots\dots (46)$$

$$G_{th\_est}(k) = \phi(k-1)^T \zeta'(k) \dots\dots (47)$$

$$R(k+1) = \frac{1}{\lambda_1''} \left[ I - \frac{\lambda_2'' \cdot R(k) \cdot \zeta'(k) \cdot \zeta'(k)^T}{\lambda_1'' + \lambda_2'' \cdot \zeta'(k)^T \cdot R(k) \cdot \zeta'(k)} \right] R(k) \\ \dots\dots (48)$$

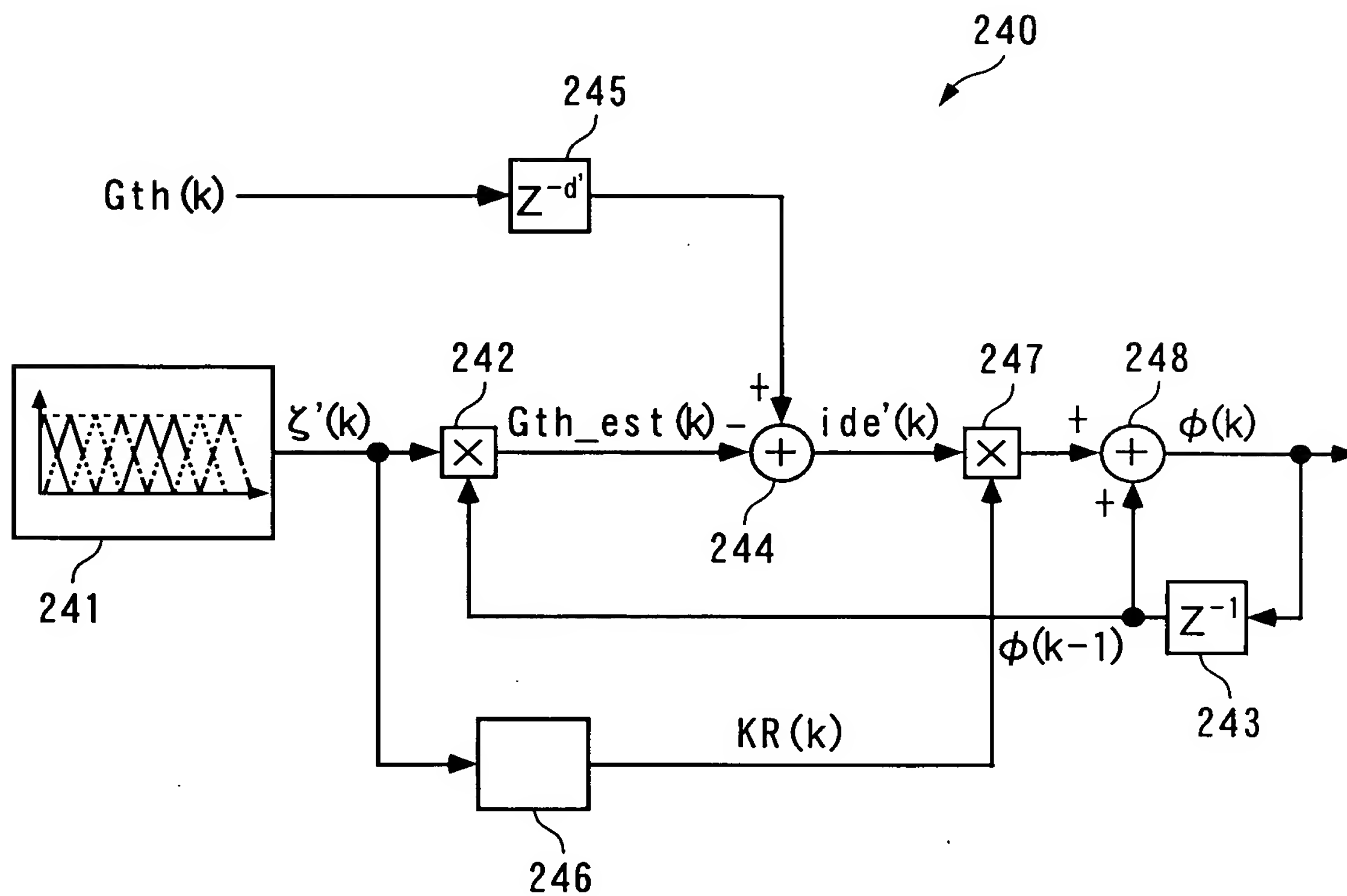
I: UNIT MATRIX  
 $\lambda_1''$ ,  $\lambda_2''$ : WEIGHTING PARAMETER

$$\phi(k)^T = [\Phi\#1(k), \Phi\#2(k), \Phi\#3(k), \Phi\#4(k)] \dots\dots (49)$$

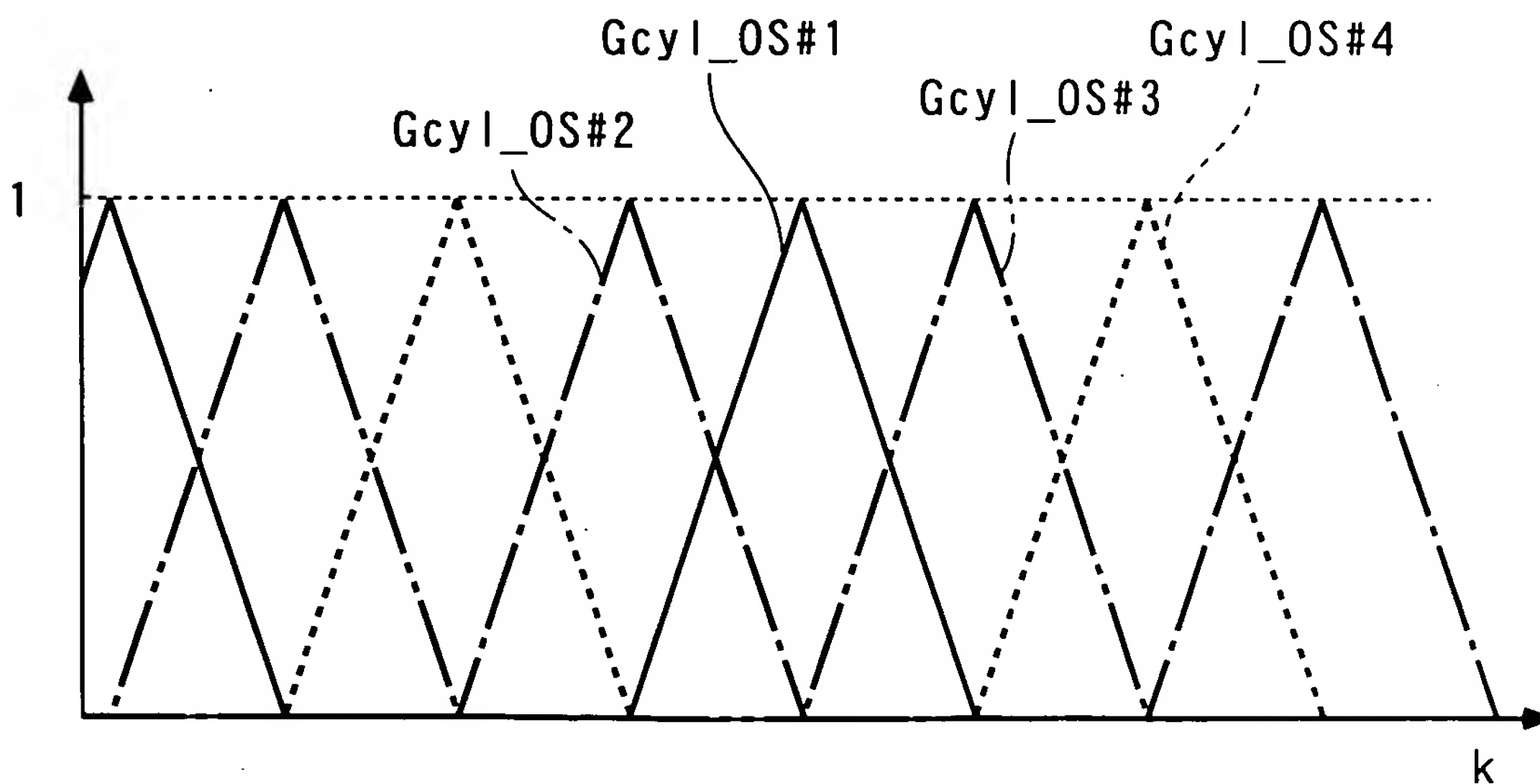
$$\zeta'(k)^T = [G_{cyl\_OS\#1}(k), G_{cyl\_OS\#2}(k), G_{cyl\_OS\#3}(k), G_{cyl\_OS\#4}(k)] \\ \dots\dots (50)$$



F I G. 3 7



F I G. 3 8



F I G. 3 9

$$E\Phi\#i(k) = \Phi\#i(k) - \Phi\#1(k) \quad \dots\dots (51)$$

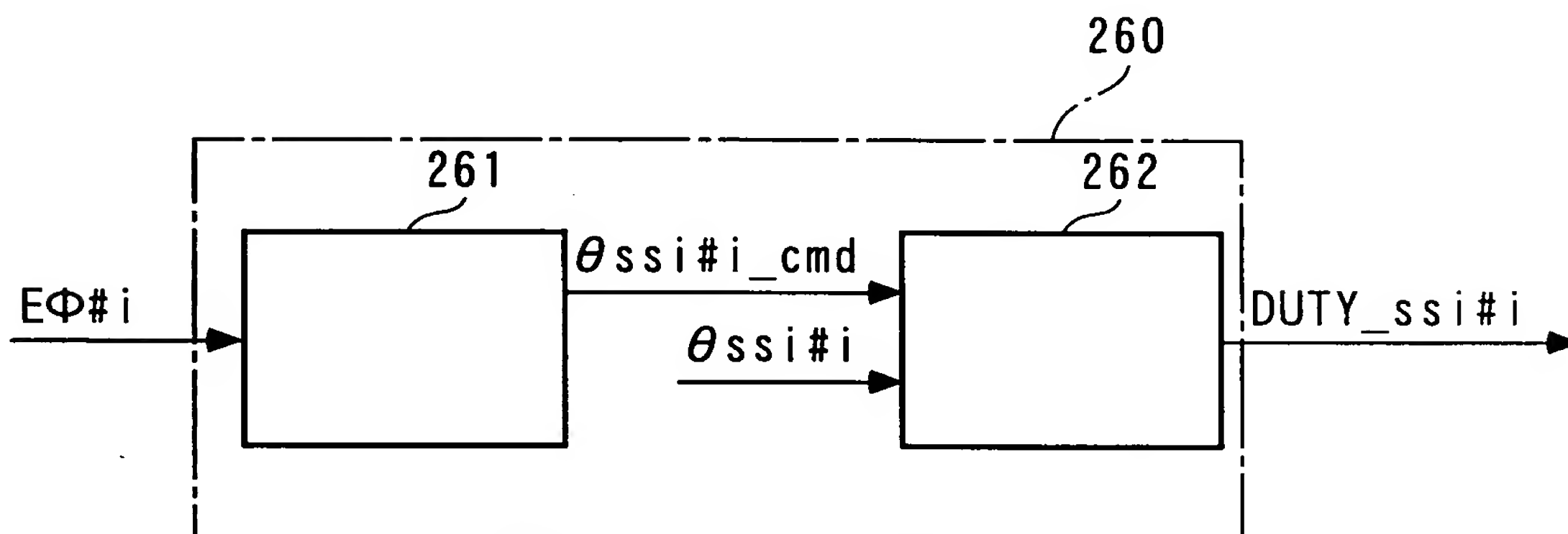
$$(i = 2 \sim 4)$$

$$\sigma'(k) = E\Phi\#i(k) + S'E\Phi\#i(k-1) \quad \dots\dots (52)$$

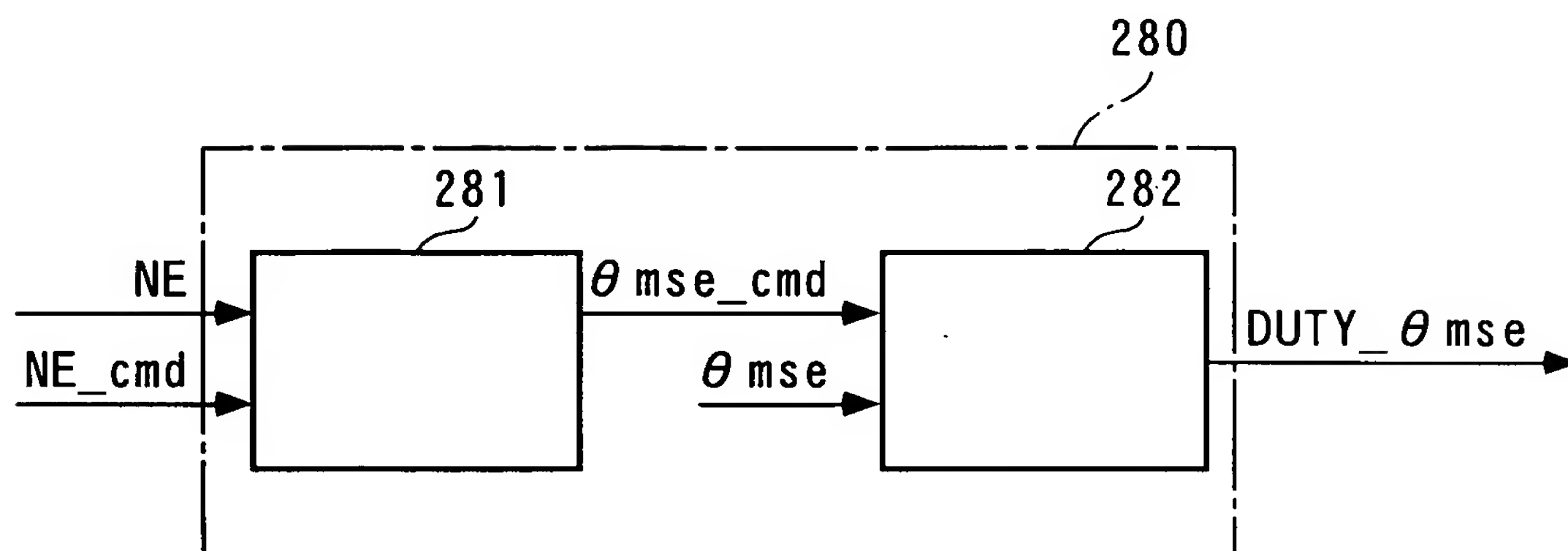
$$\theta_{ss\#i\_cmd}(k) = -Fs' \cdot \sigma'(k) - Gs' \cdot \sum_{j=0}^k \sigma'(j) - Hs' \cdot E\Phi\#i(k) \quad \dots\dots (53)$$

$Fs', Gs', Hs'$  : FEEDBACK GAIN  
 $S'$  : SWITCHING FUNCTION-SETTING PARAMETER ( $-1 < S' < 1$ )

F I G. 4 0



F I G. 4 1



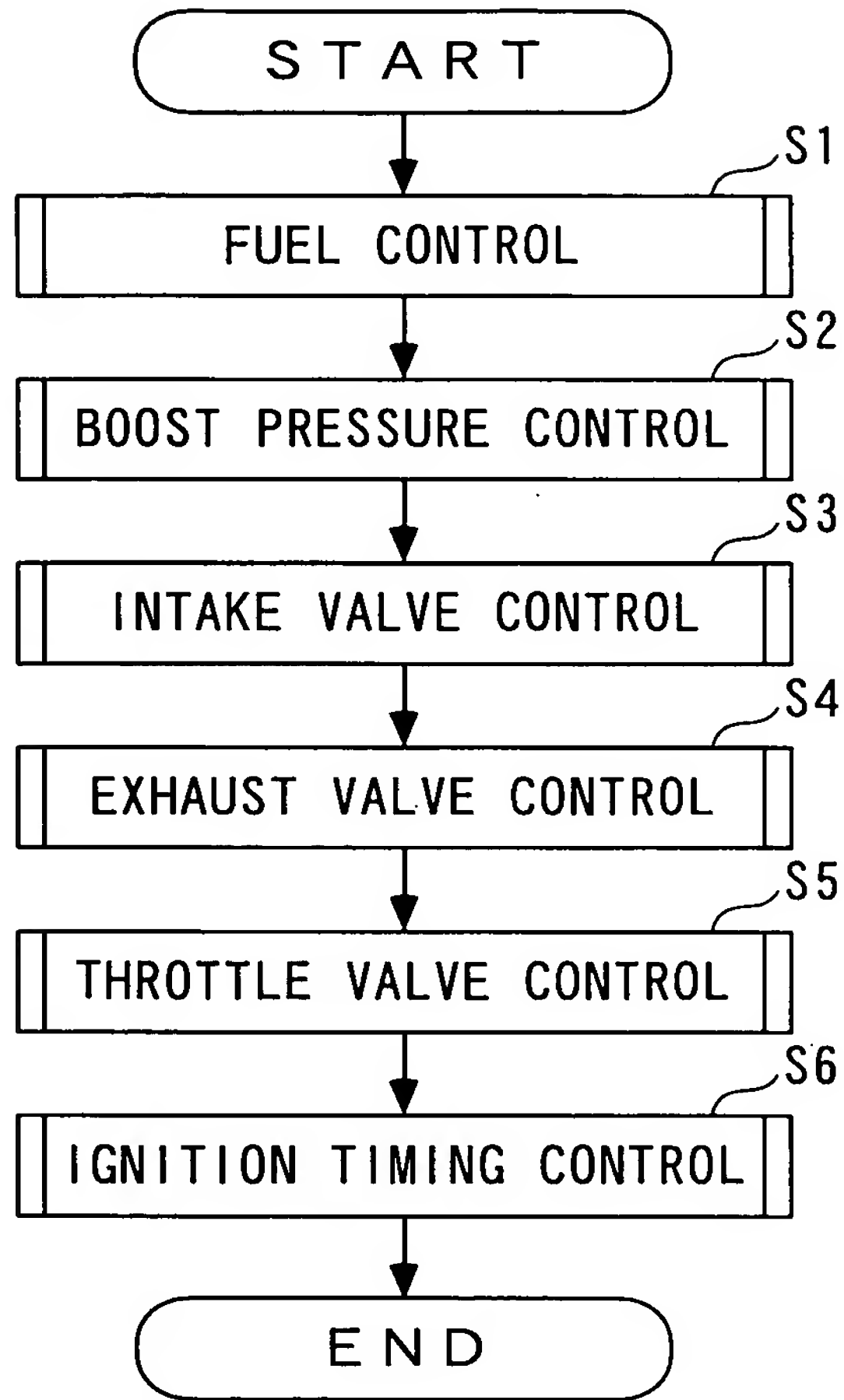
F I G. 4 2

$$\theta_{mse\_cmd}(n) = \theta_{mse\_ast}(n) + d\theta_{mse}(n) \quad \dots\dots (54)$$

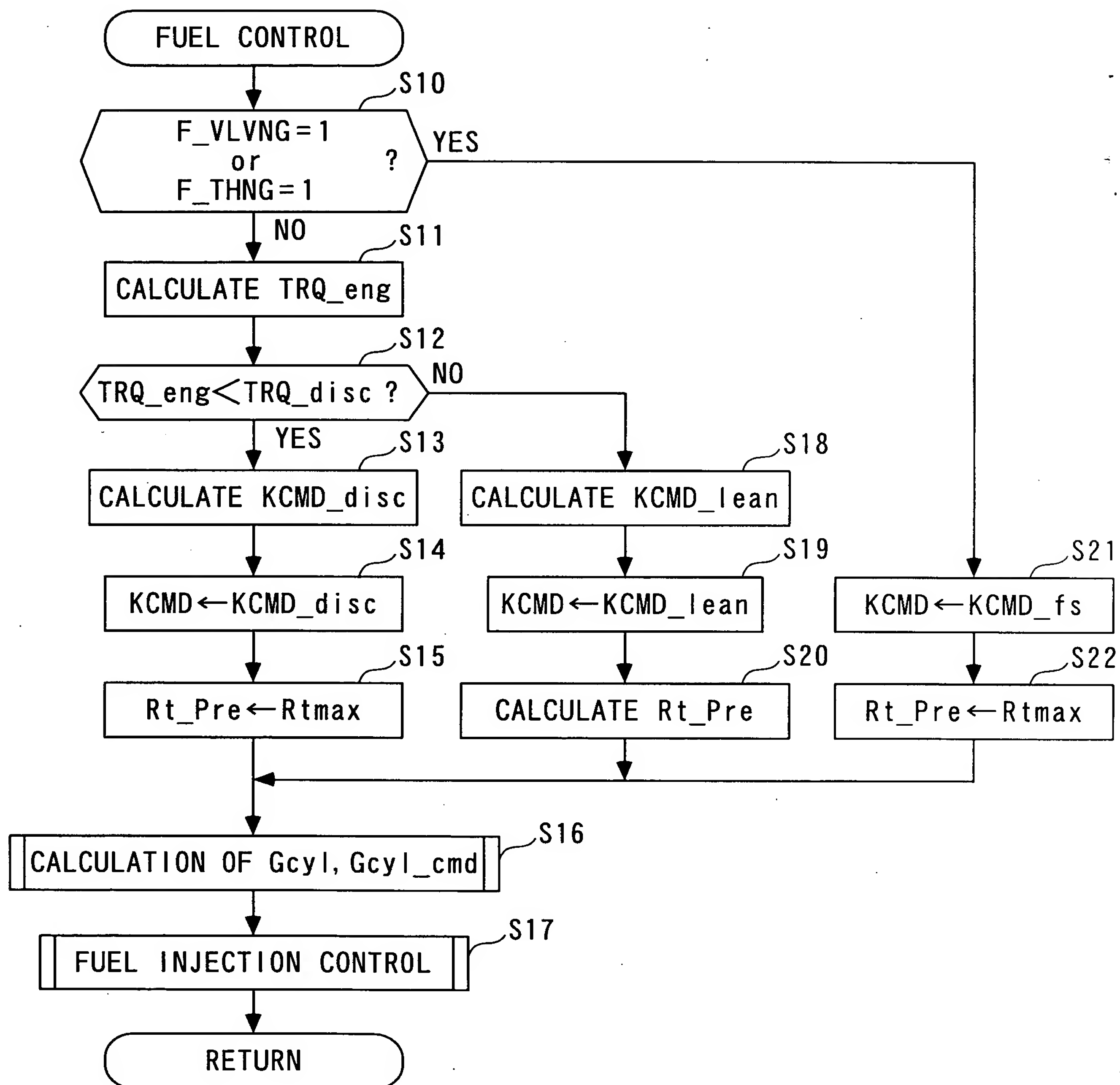
$$d\theta_{mse}(n) = -K_{astr} \cdot \sigma_{ast}(n) + \left[ -K_{asta} \cdot \sum_{i=0}^n \sigma_{ast}(i) \right] \quad \dots\dots (55)$$

$$\sigma_{ast}(n) = NE(n) - NE\_cmd(n) + S_{ast} \cdot [NE(n-1) - NE\_cmd(n-1)] \quad \dots\dots (56)$$

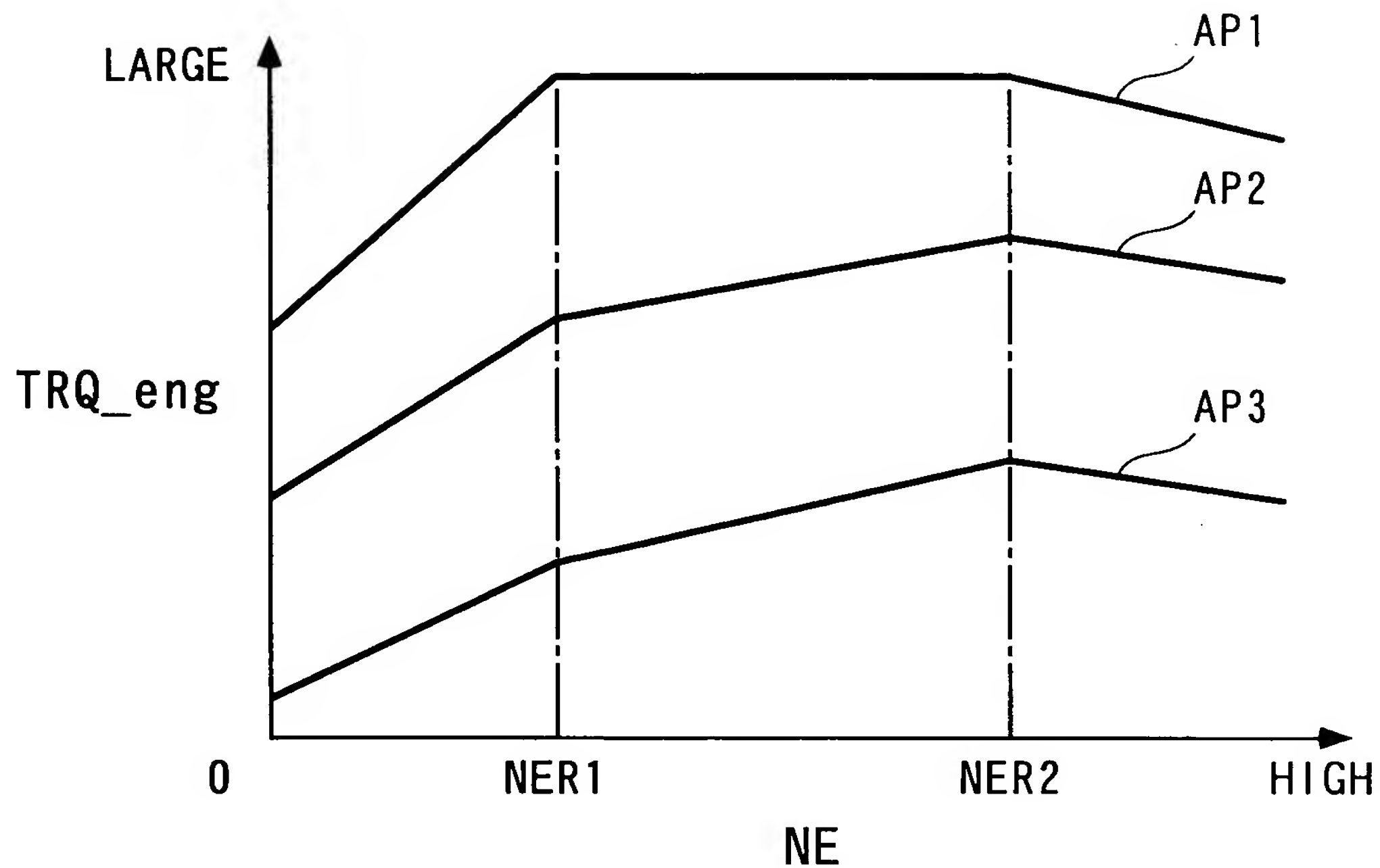
F I G. 4 3



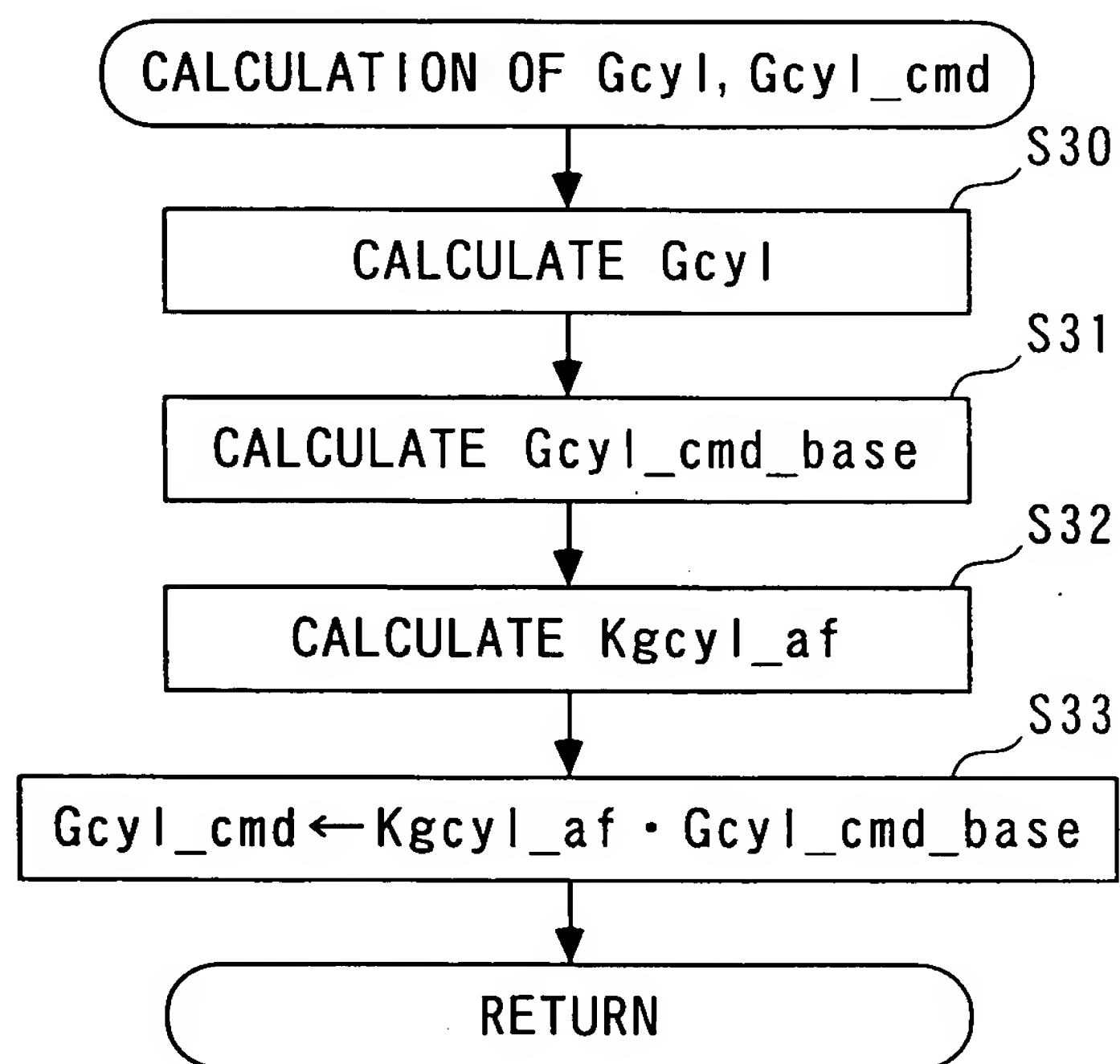
F I G . 4 4



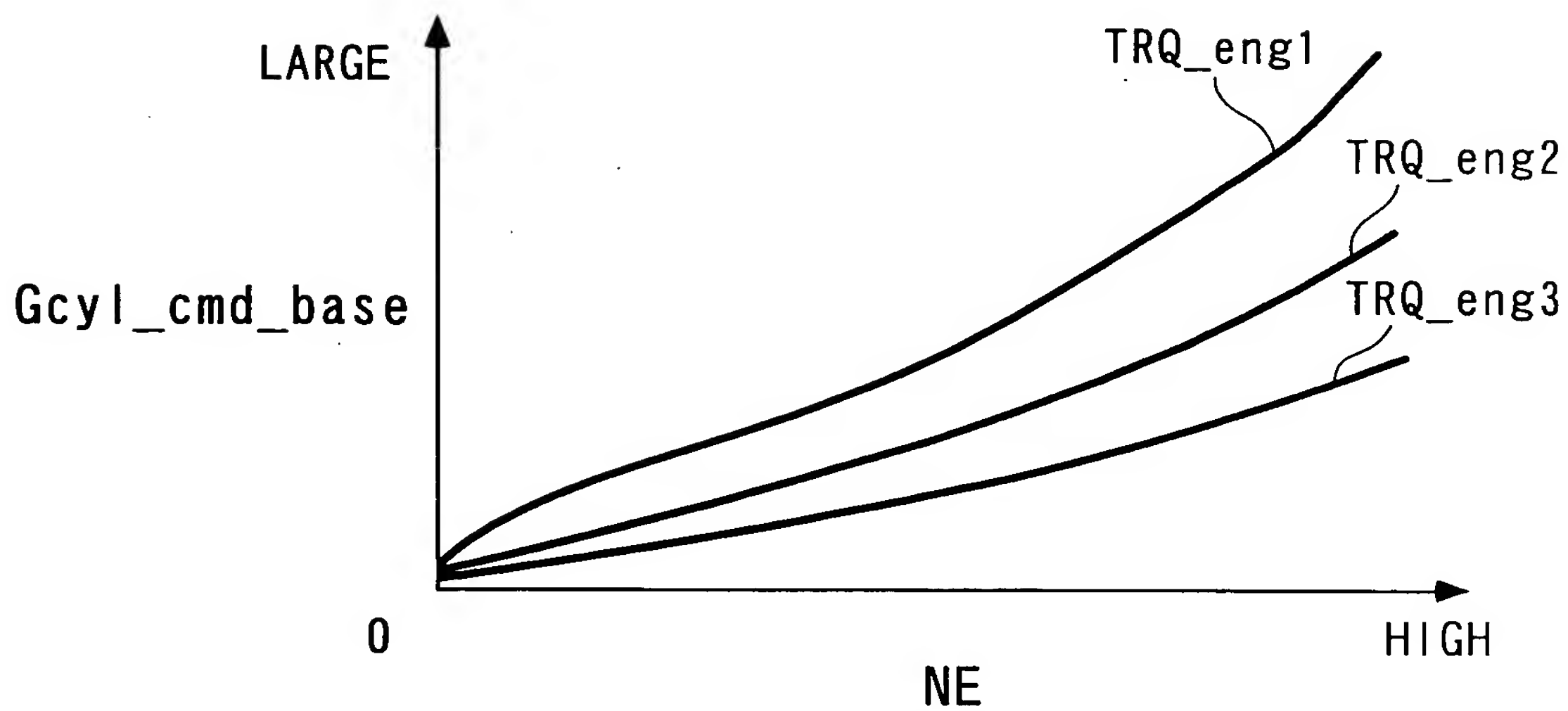
F I G . 4 5



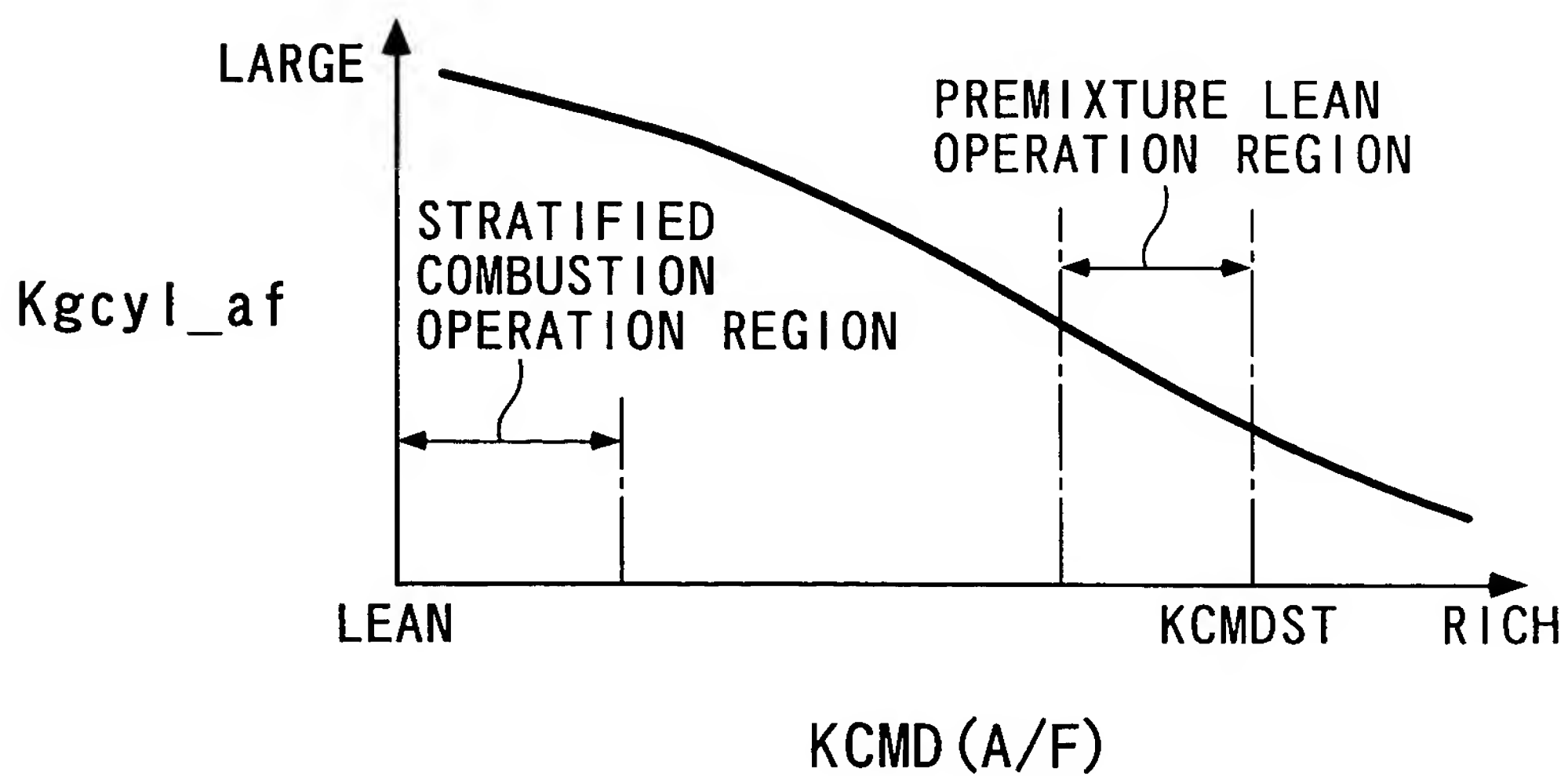
F I G . 4 6



F I G . 4 7



F I G . 4 8



F I G . 4 9

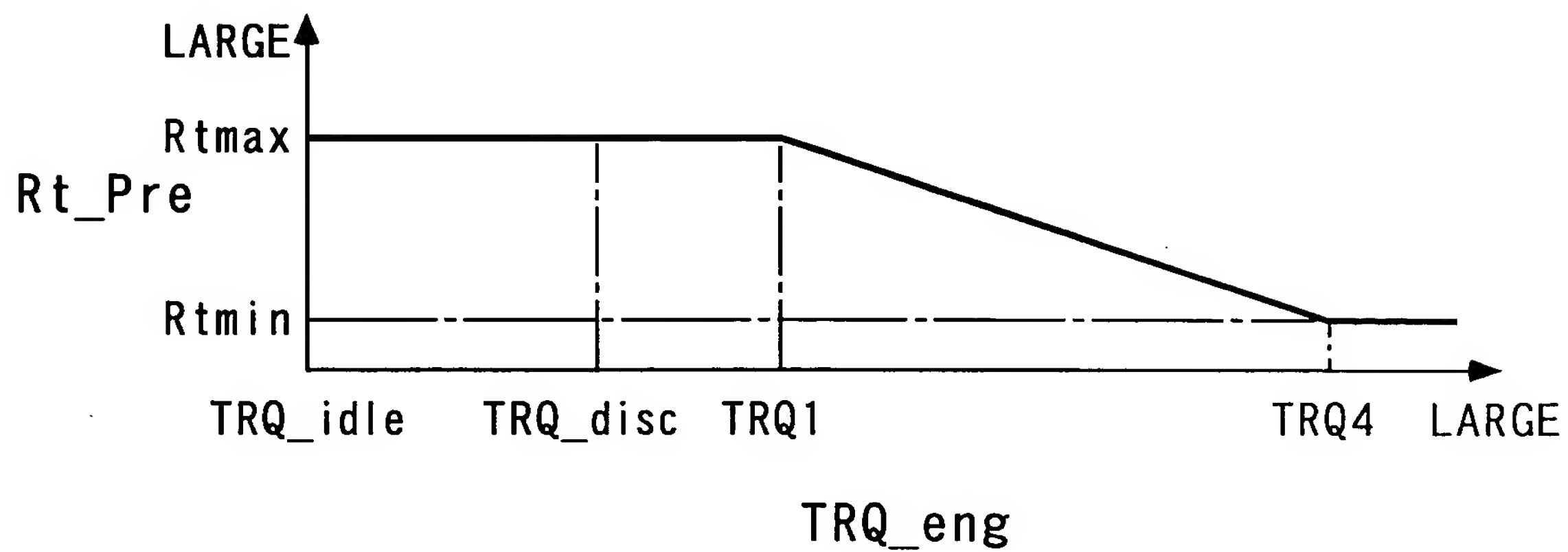
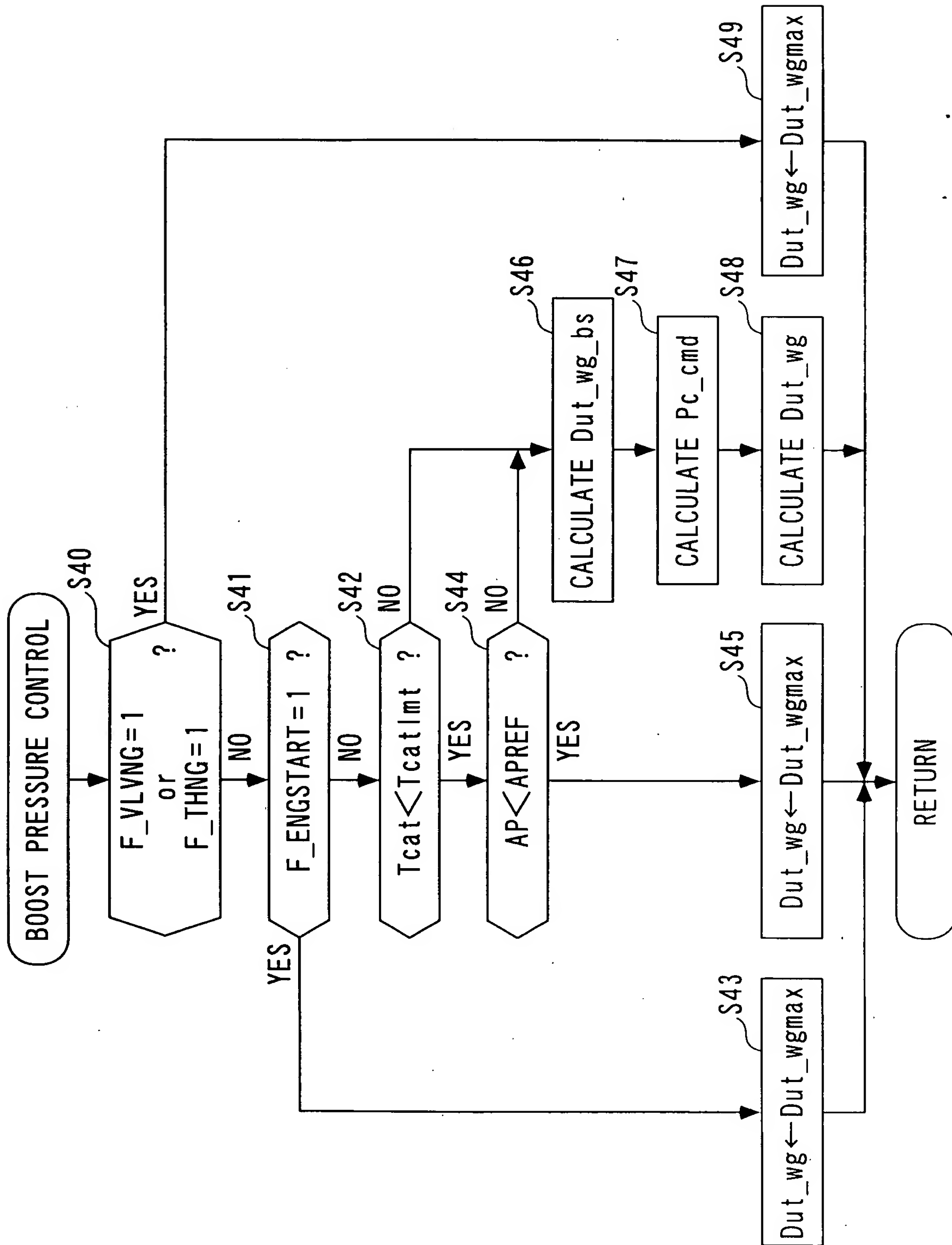
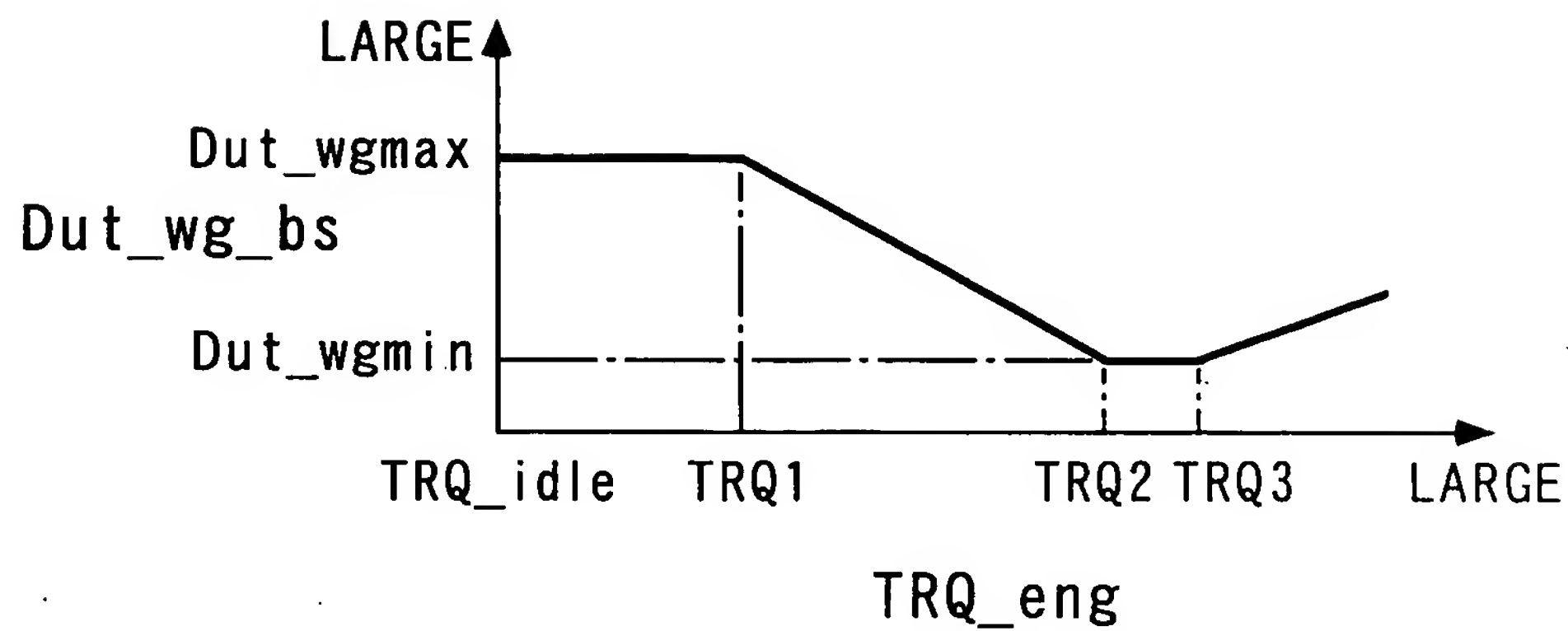




FIG. 50



F I G. 5 1



F I G. 5 2

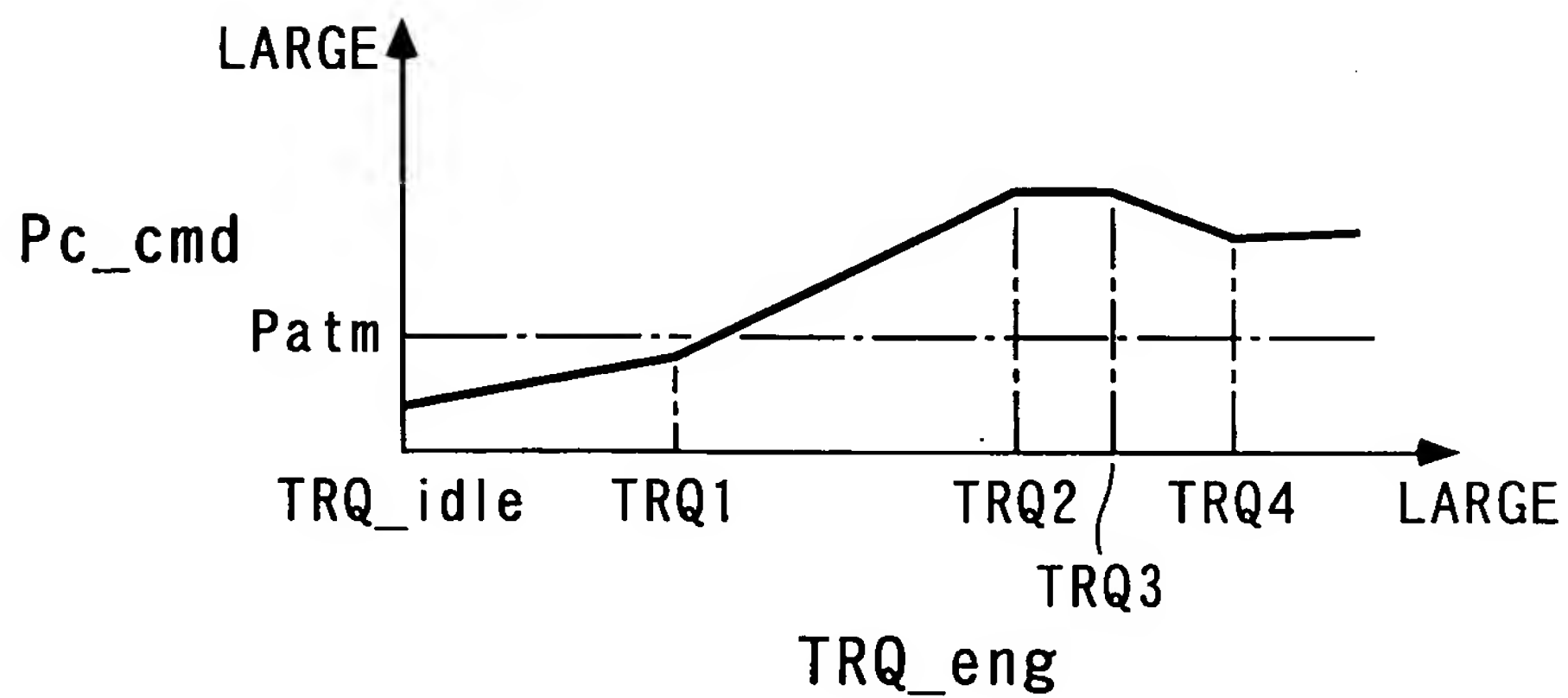
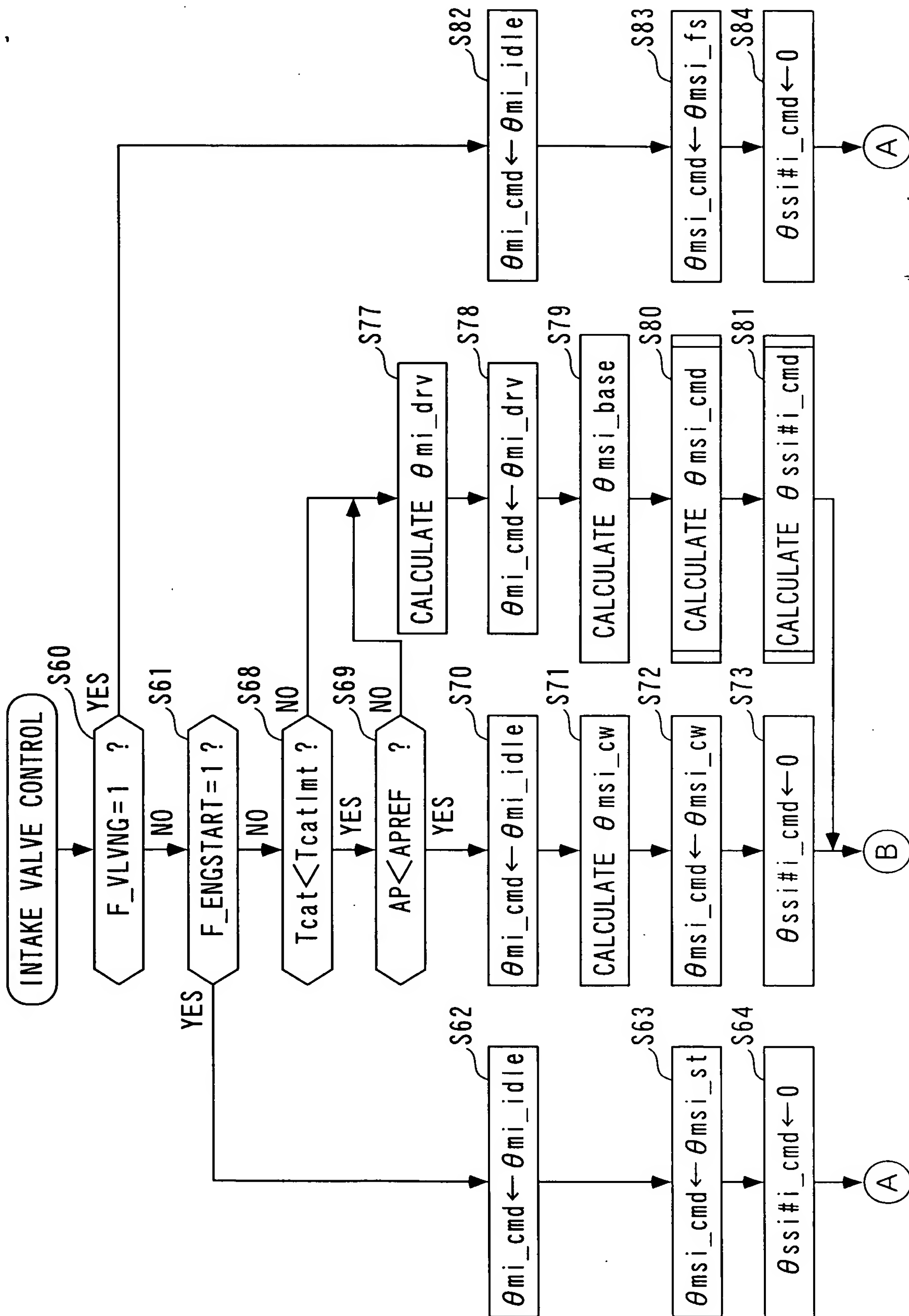
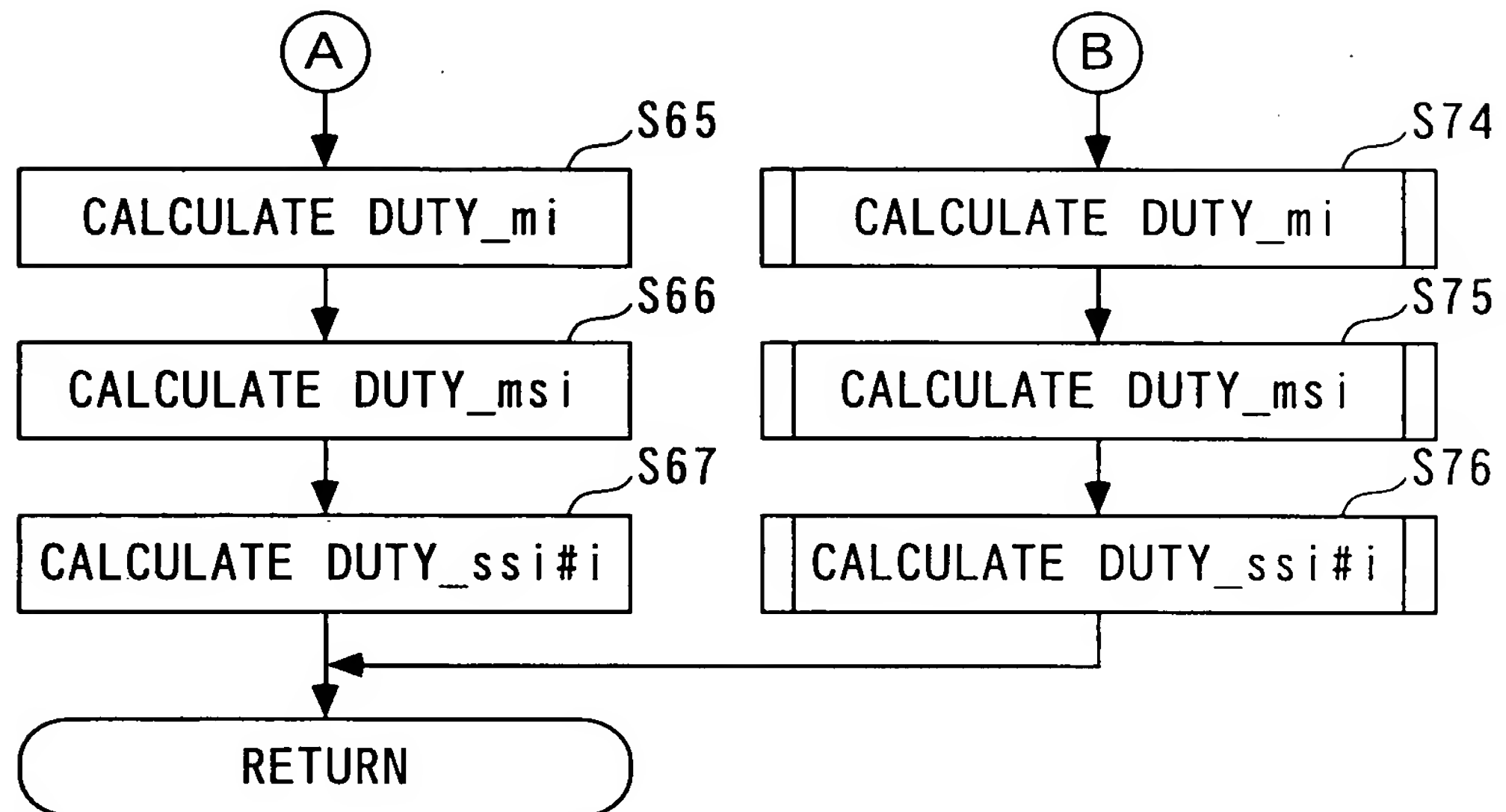


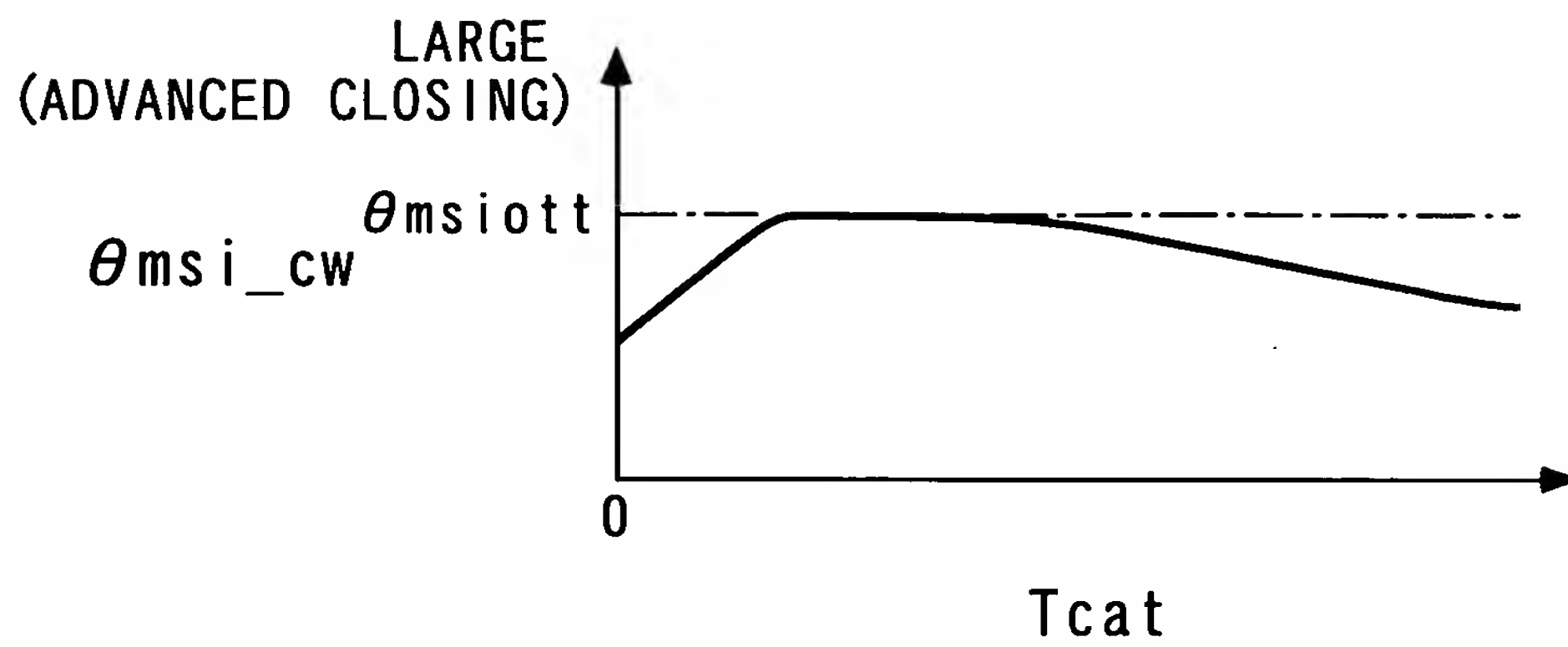
FIG. 53



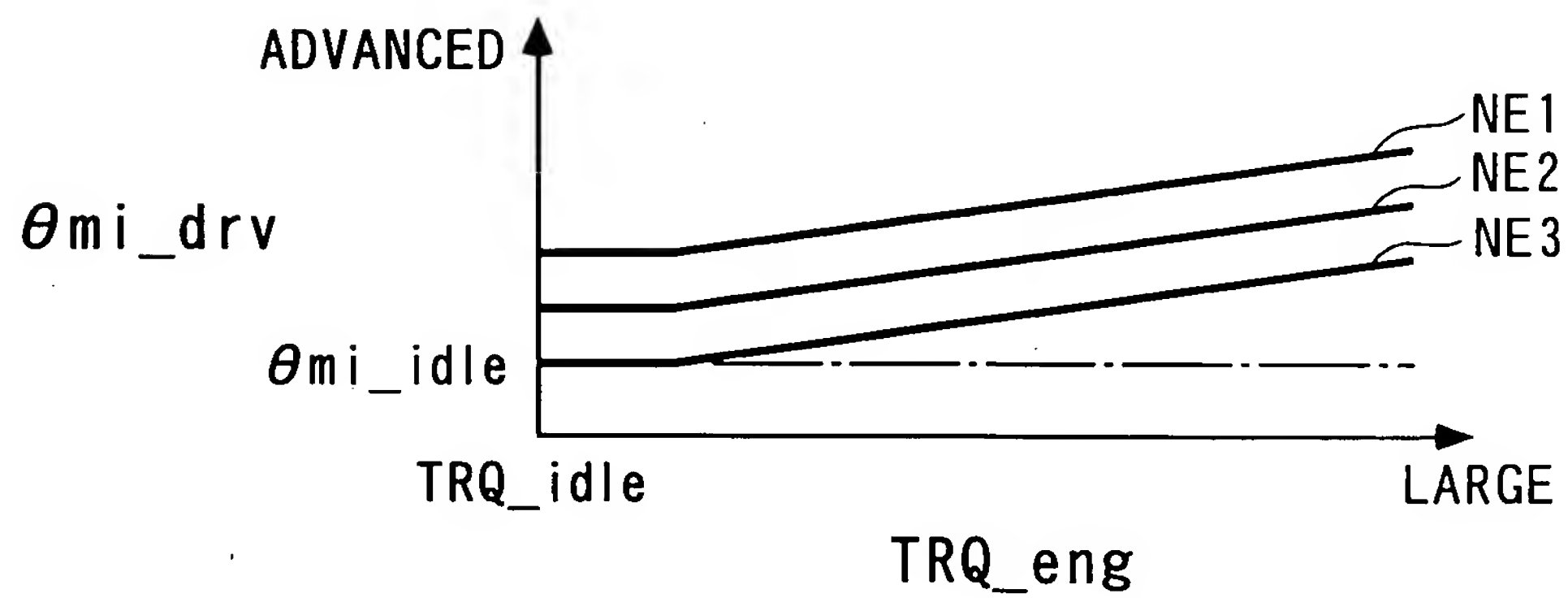
F I G . 5 4



F I G . 5 5



F I G . 5 6



F I G. 5 7

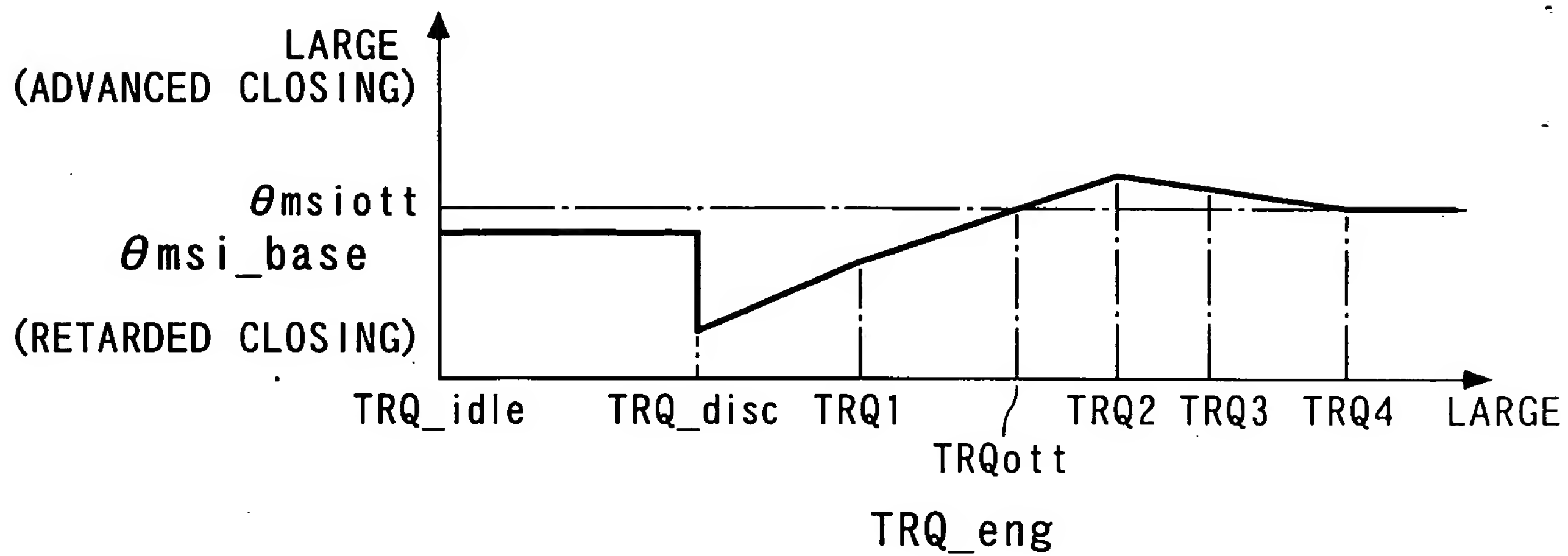
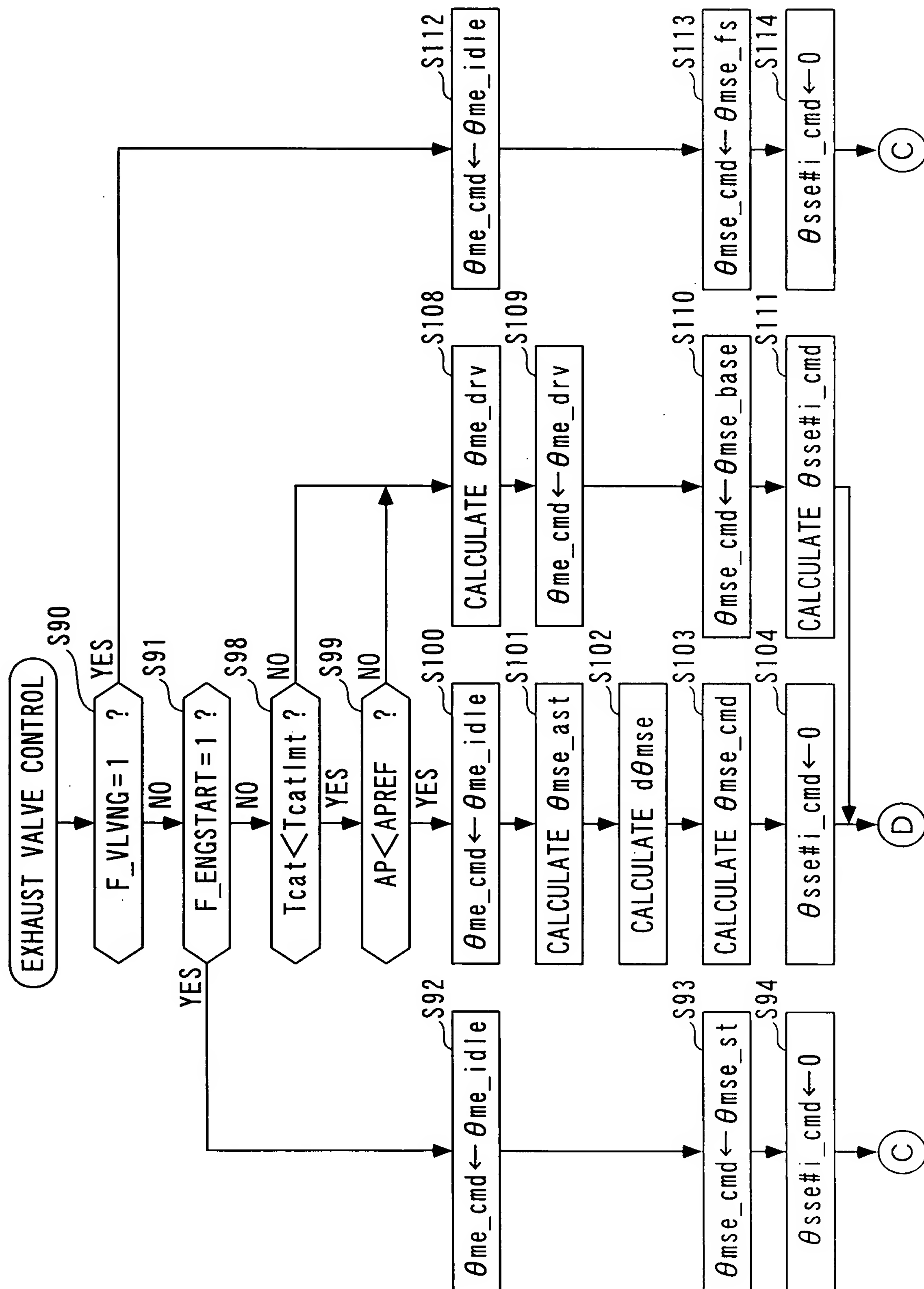
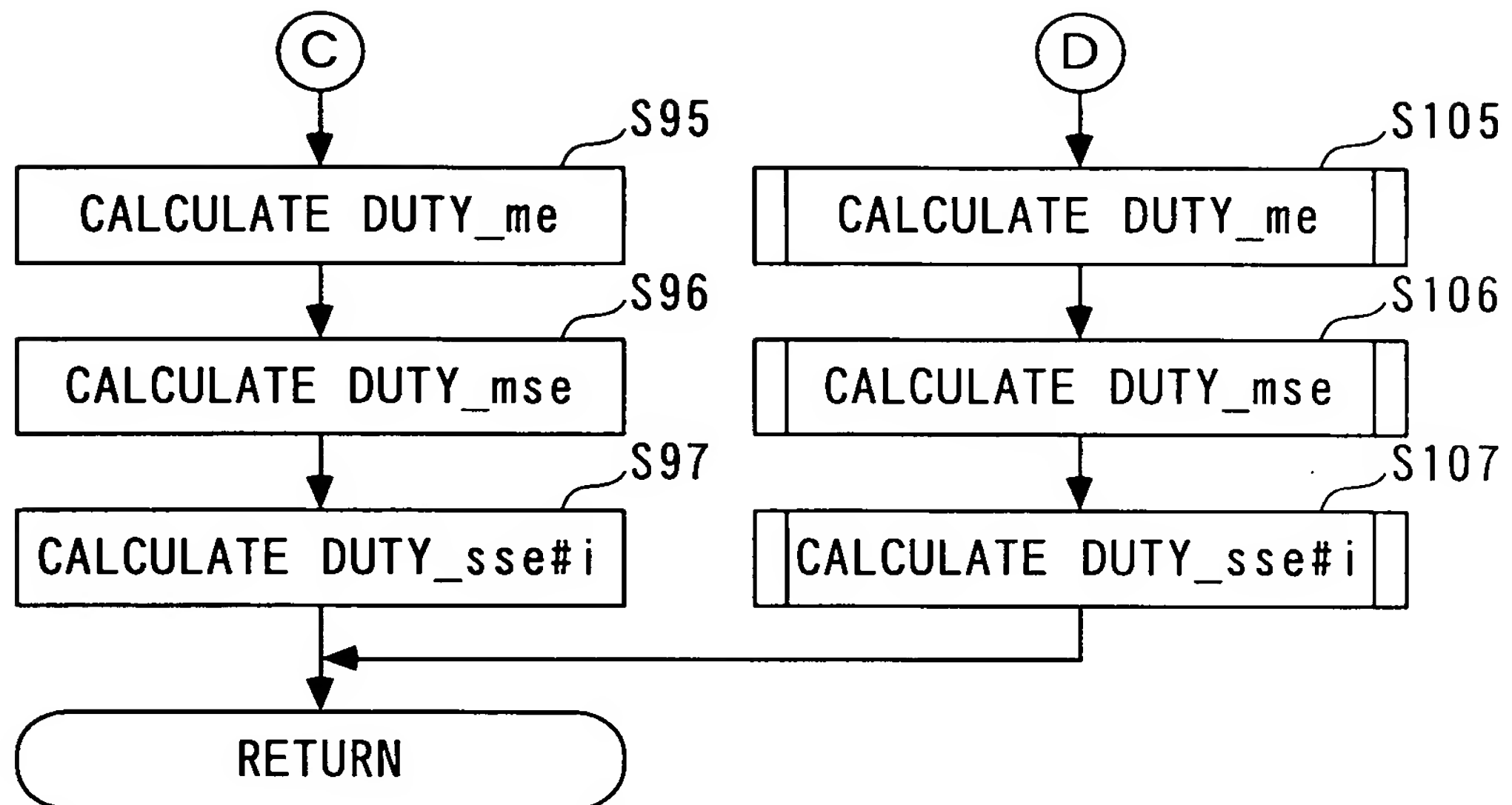


FIG. 58

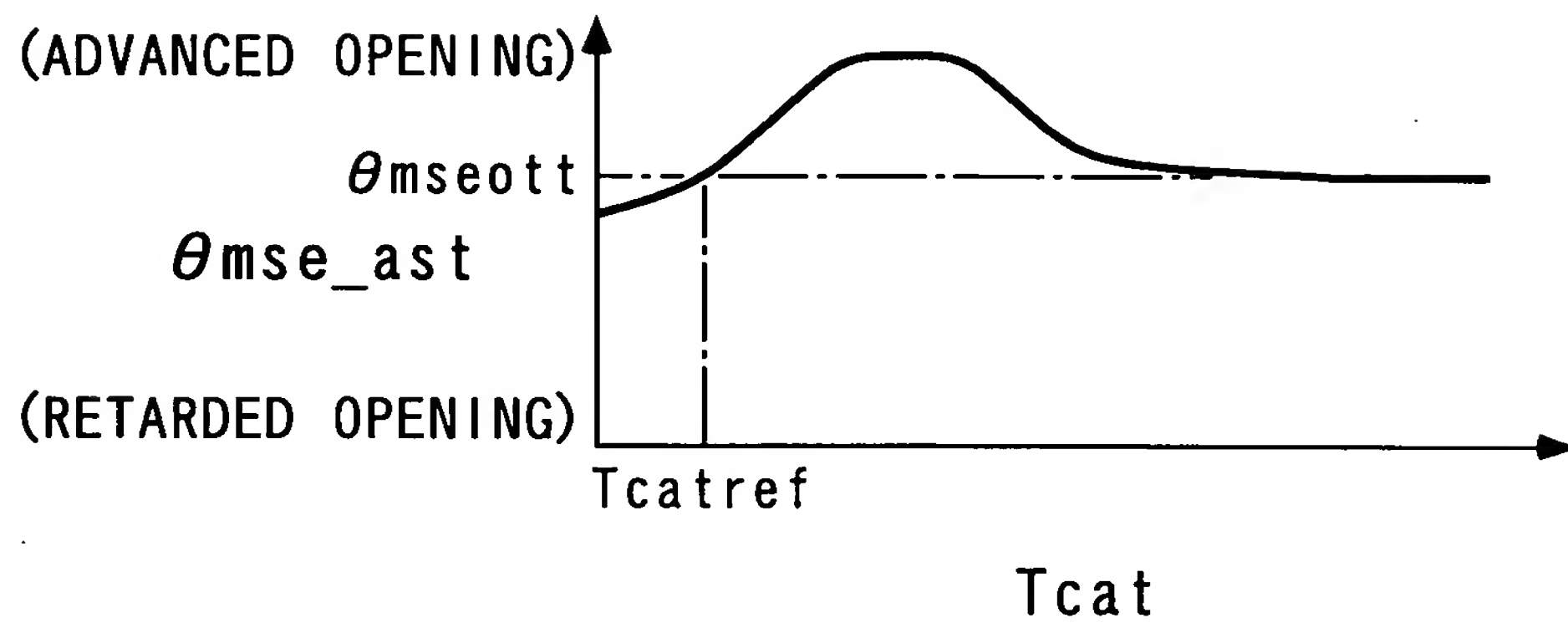


F I G. 5 9





F I G. 6 0



F I G. 6 1

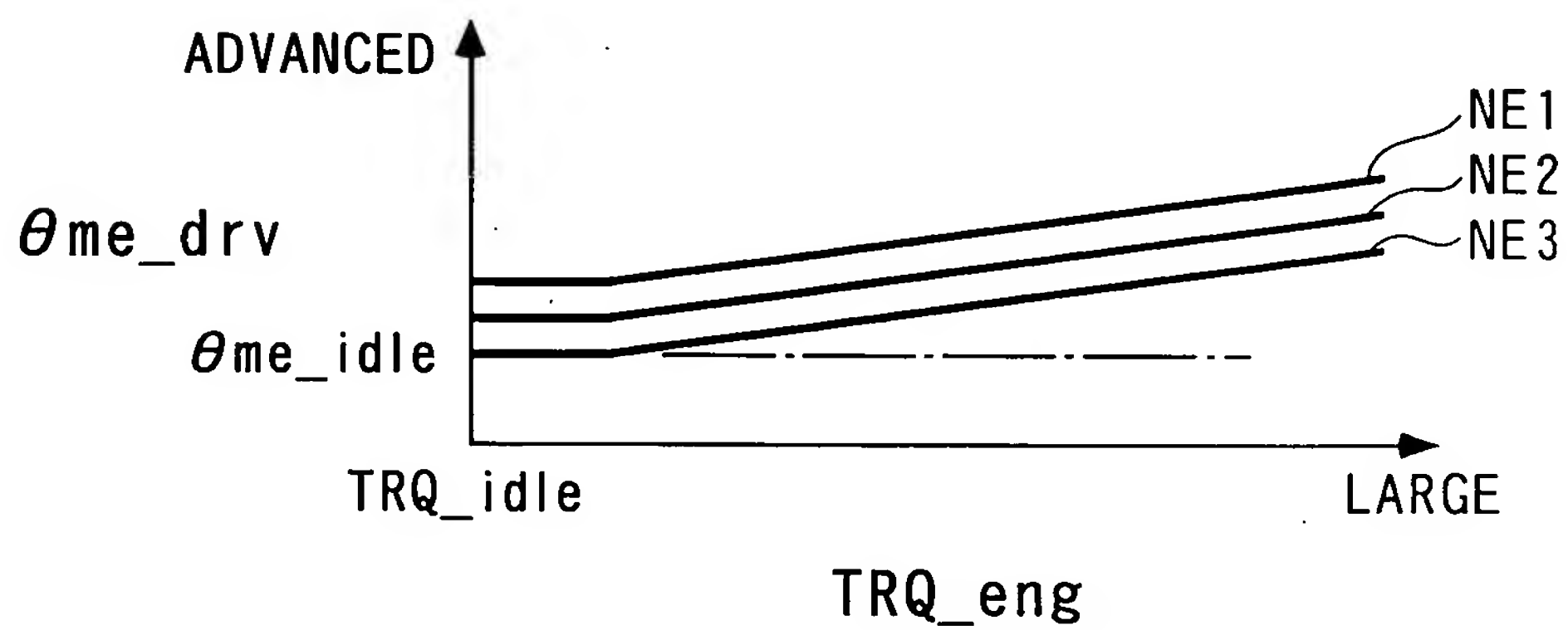
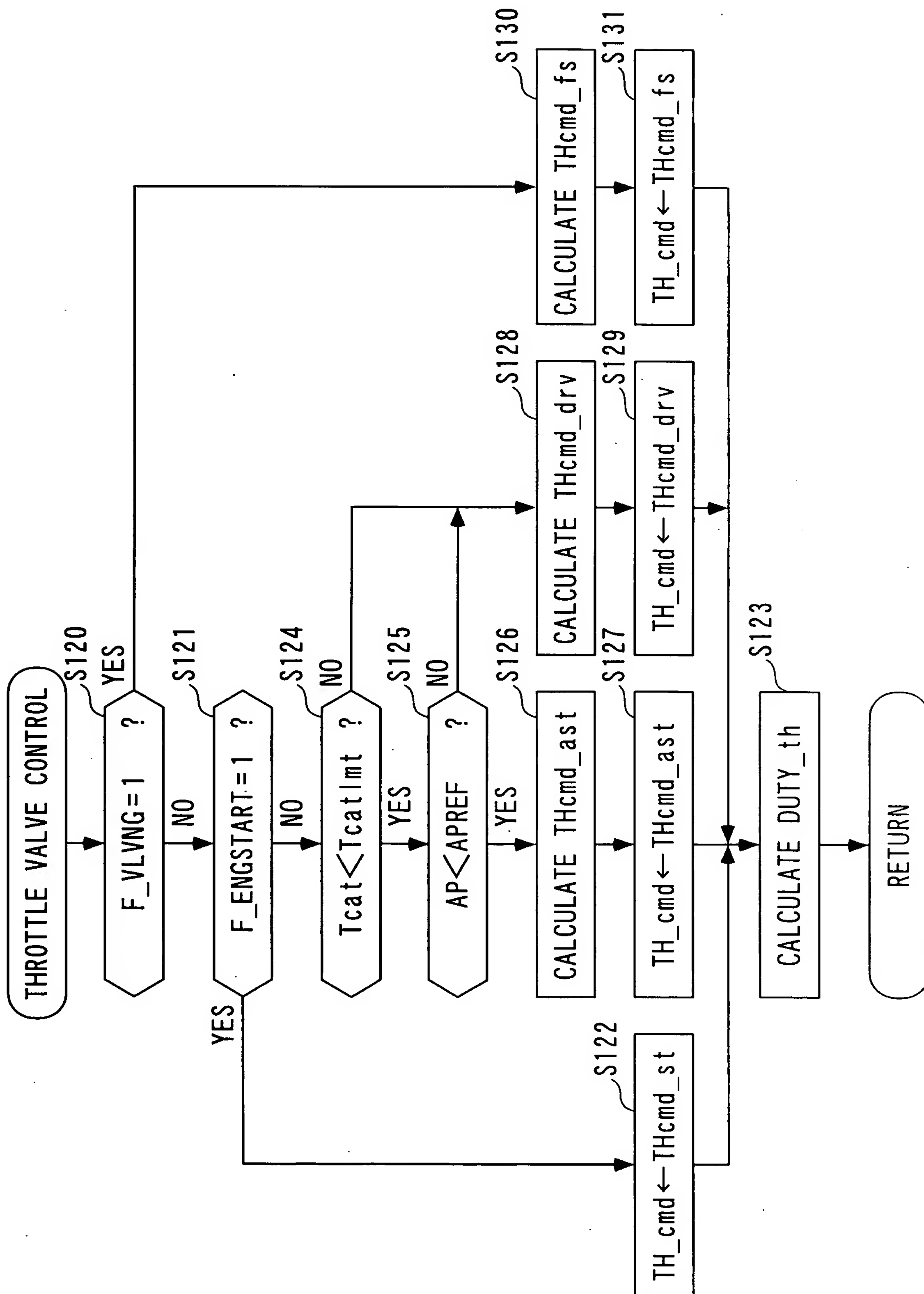
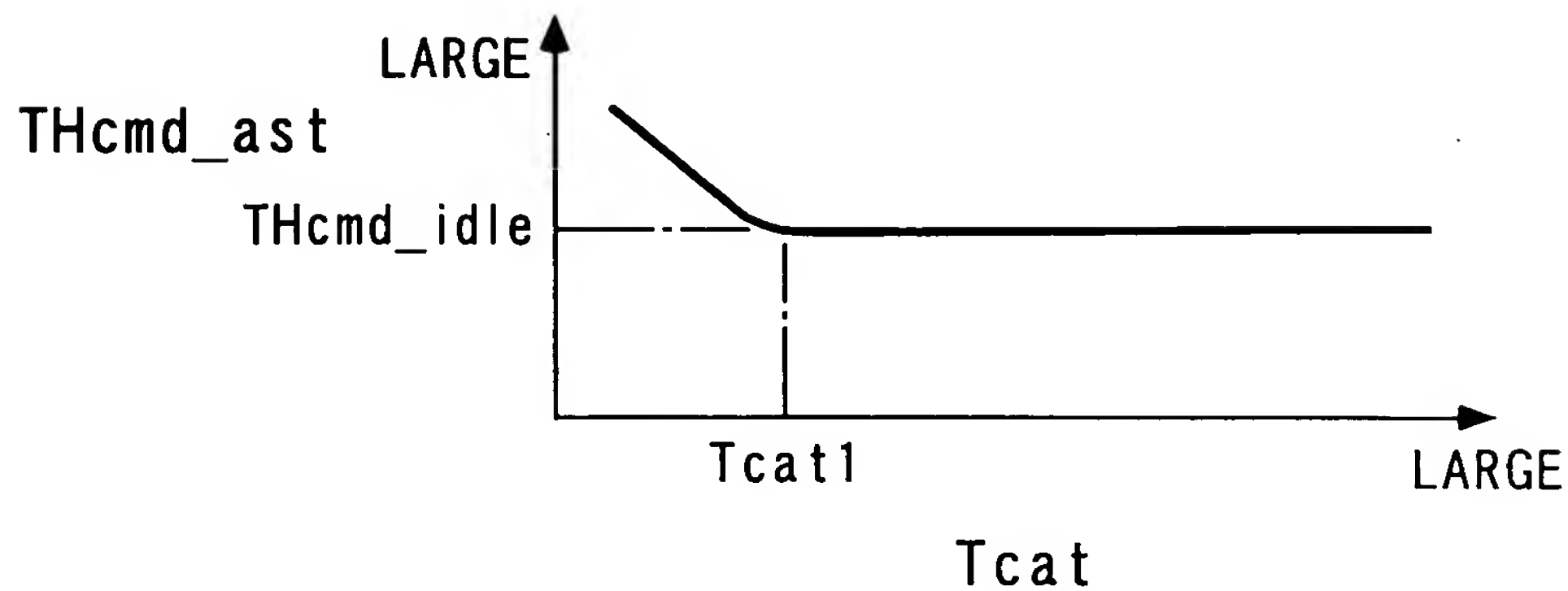


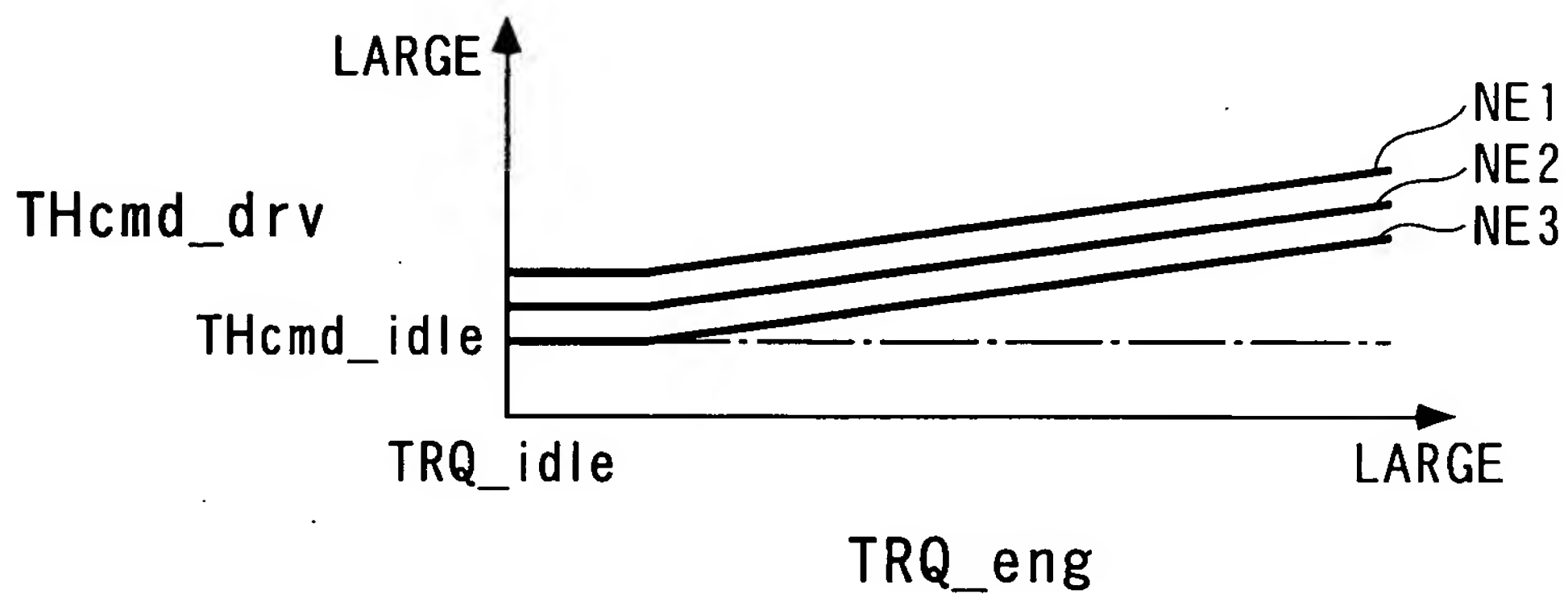
FIG. 62



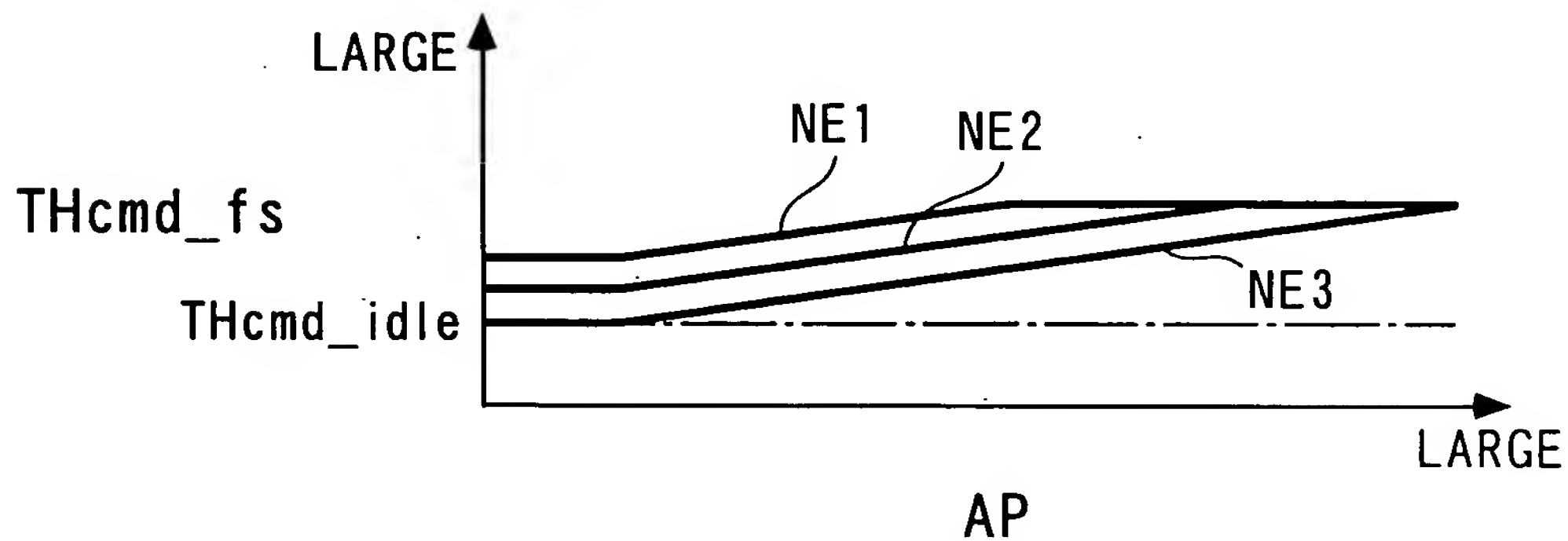
F I G . 6 3



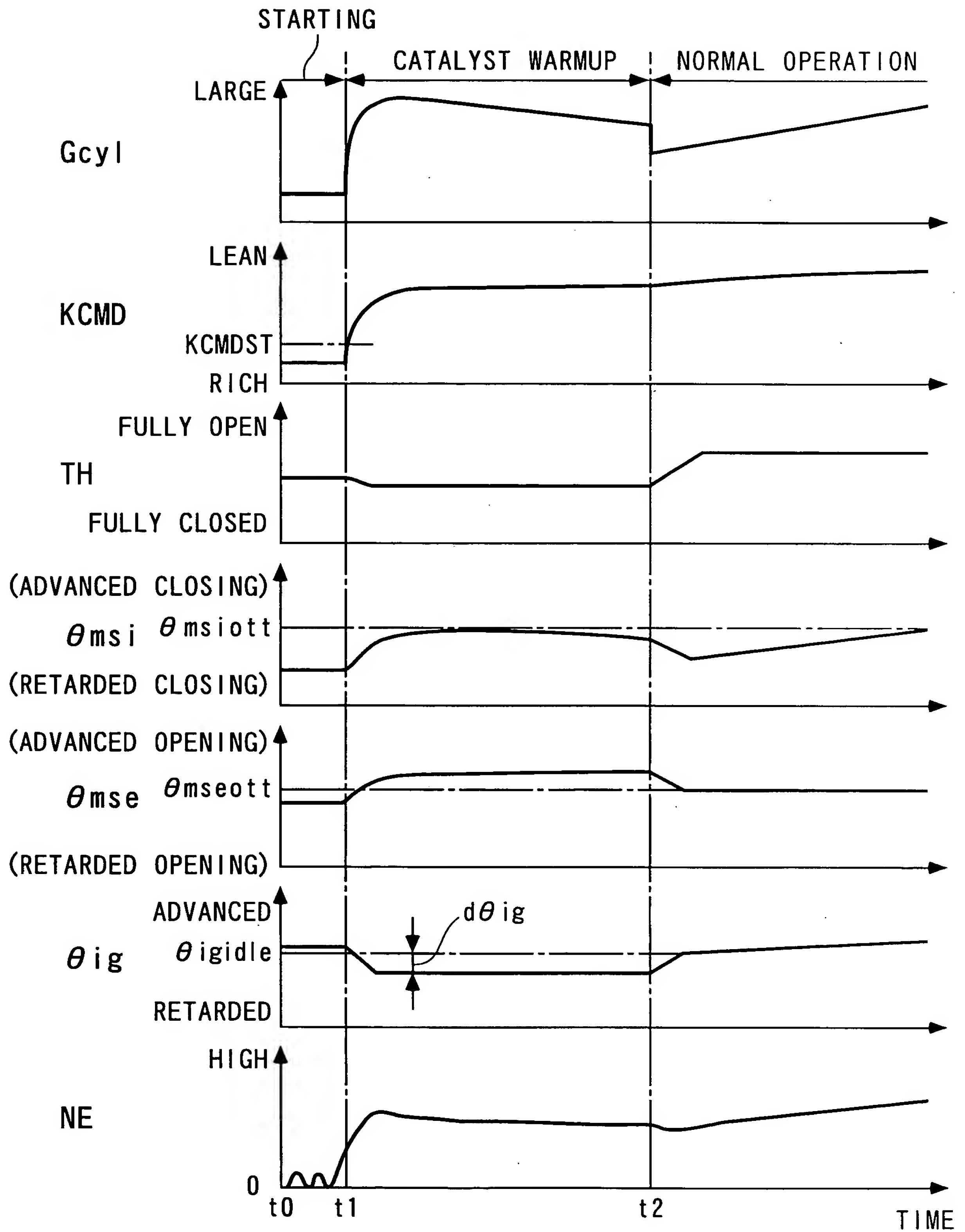
F I G . 6 4



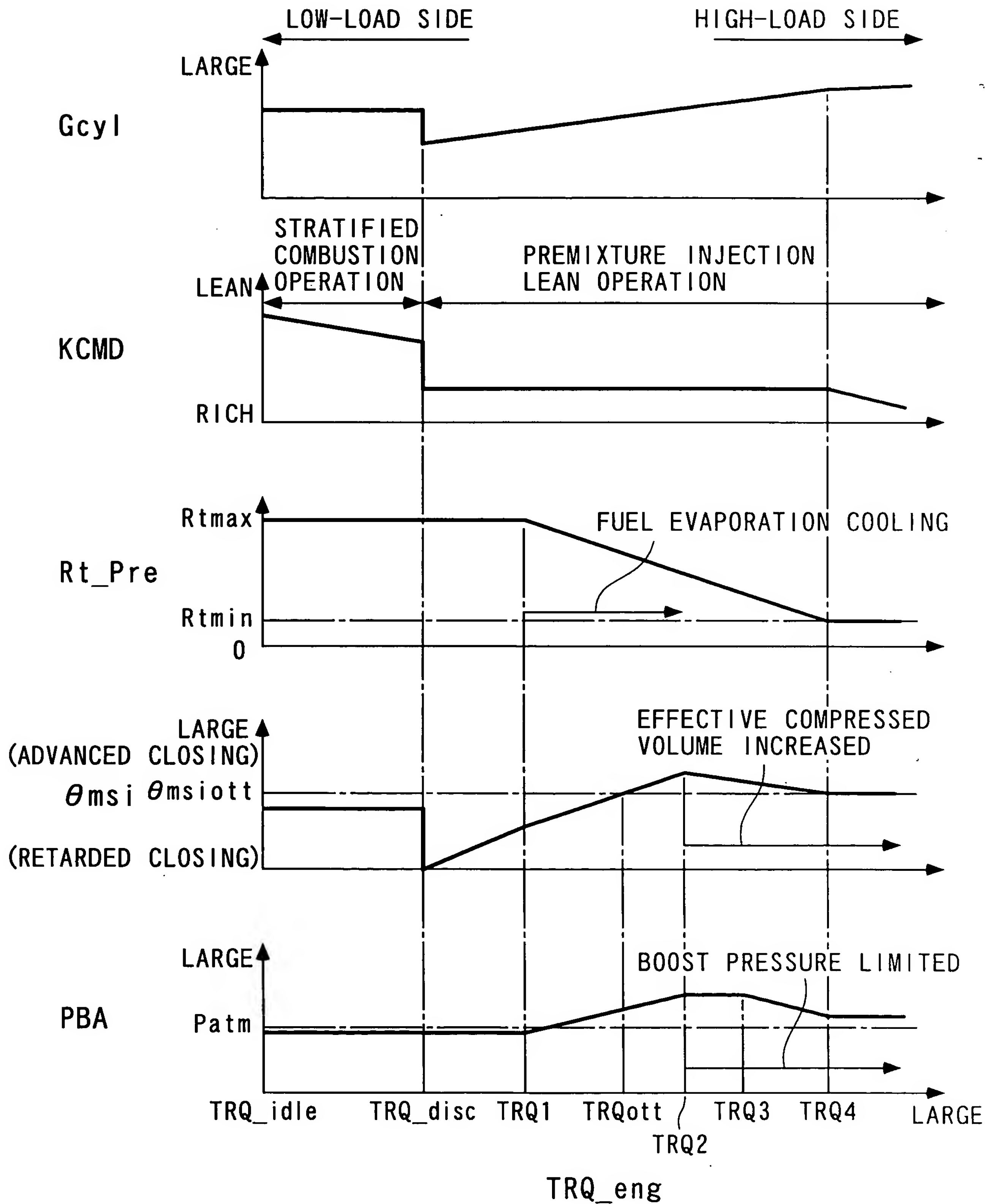
F I G . 6 5



F I G . 6 6



F I G . 6 7



**F I G. 68**

